

Regulations Compliance Report

Approved Document L1A, 2013 Edition, England assessed by Stroma FSAP 2012 program, Version: 1.0.4.26
Printed on 01 September 2020 at 16:56:33

Project Information:

Assessed By: Demi Beneke (STRO027754)

Building Type: Detached House

Dwelling Details:

NEW DWELLING DESIGN STAGE

Total Floor Area: 114.94m²

Site Reference : Land Adj 11 Queen Annes Drive 6384

Plot Reference: Land Adj 11 Queen Annes Drive

Address : Land Adj 11 Queen Annes Drive

Client Details:

Name:

Address :

This report covers items included within the SAP calculations.

It is not a complete report of regulations compliance.

1a TER and DER

Fuel for main heating system: Mains gas

Fuel factor: 1.00 (mains gas)

Target Carbon Dioxide Emission Rate (TER) 18.41 kg/m²

Dwelling Carbon Dioxide Emission Rate (DER) 18.24 kg/m²

OK

1b TFEE and DFEE

Target Fabric Energy Efficiency (TFEE) 62.3 kWh/m²

Dwelling Fabric Energy Efficiency (DFEE) 54.3 kWh/m²

OK

2 Fabric U-values

Element	Average	Highest	
External wall	0.19 (max. 0.30)	0.19 (max. 0.70)	OK
Floor	0.17 (max. 0.25)	0.22 (max. 0.70)	OK
Roof	0.11 (max. 0.20)	0.11 (max. 0.35)	OK
Openings	1.43 (max. 2.00)	1.80 (max. 3.30)	OK

2a Thermal bridging

Thermal bridging calculated from linear thermal transmittances for each junction

3 Air permeability

Air permeability at 50 pascals 5.00 (design value)
Maximum 10.0

OK

4 Heating efficiency

Main Heating system: Database: (rev 464, product index 017929):
Boiler systems with radiators or underfloor heating - mains gas
Brand name: Ideal
Model: LOGIC COMBI
Model qualifier: ESP1 35
(Combi)
Efficiency 89.6 % SEDBUK2009
Minimum 88.0 %

OK

Secondary heating system: None

Regulations Compliance Report

5 Cylinder insulation

Hot water Storage: No cylinder

6 Controls

Space heating controls: Programmer, room thermostat and TRVs **OK**
 Hot water controls: No cylinder thermostat

No cylinder
 Boiler interlock: Yes **OK**

7 Low energy lights

Percentage of fixed lights with low-energy fittings: 100.0%
 Minimum: 75.0% **OK**

8 Mechanical ventilation

Not applicable

9 Summertime temperature

Overheating risk (South England): Slight **OK**

Based on:

Overshading: Average or unknown
 Windows facing: North 2.25m²
 Windows facing: North 0.43m²
 Windows facing: North 2.25m²
 Windows facing: South 3.49m²
 Windows facing: West 4.53m²
 Windows facing: South 6.9m²
 Windows facing: East 1.73m²
 Windows facing: North 2.25m²
 Windows facing: North 2.25m²
 Windows facing: North 2.25m²
 Windows facing: South 1.05m²
 Windows facing: South 1.05m²
 Windows facing: South 1.05m²
 Ventilation rate: 4.00
 Blinds/curtains: None

10 Key features

Thermal bridging: 0.036 W/m²K
 Roofs U-value: 0.11 W/m²K

Predicted Energy Assessment



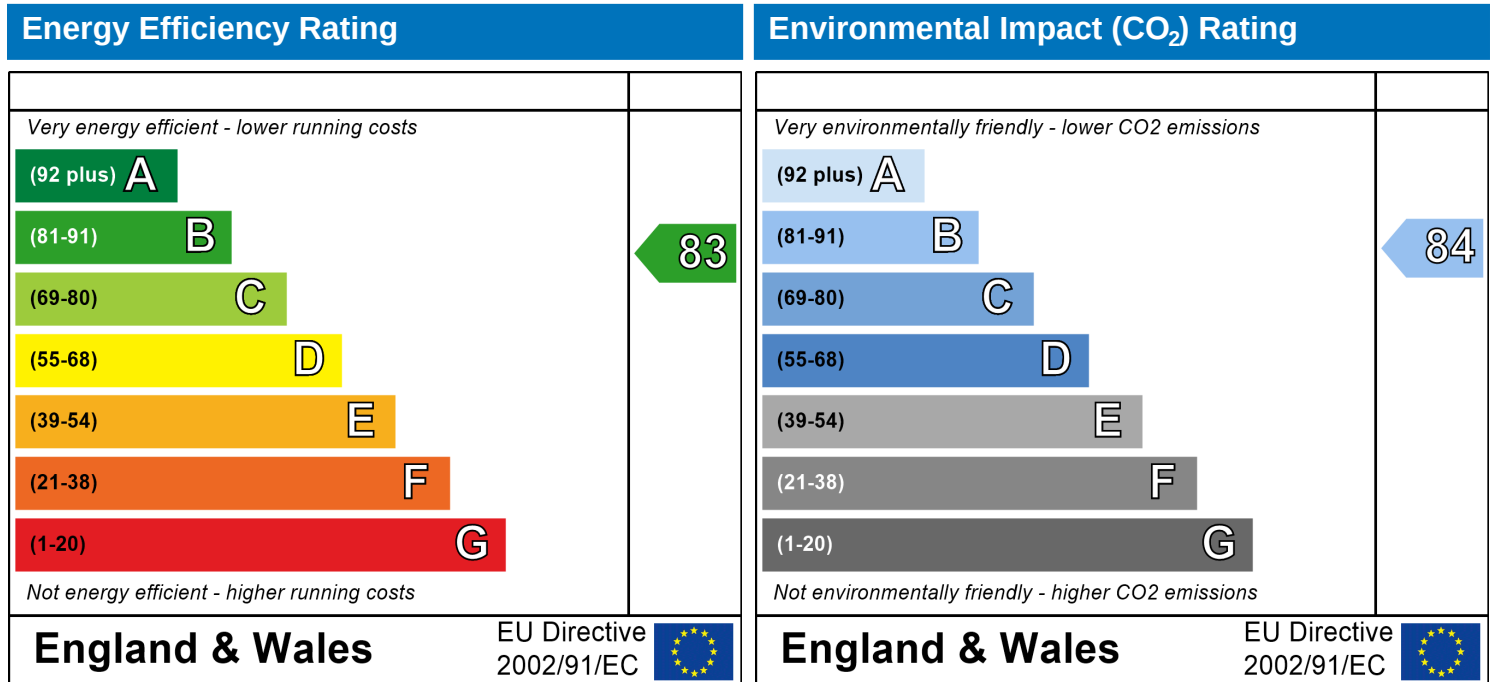
Land Adj 11 Queen Annes Drive

Dwelling type:
Date of assessment:
Produced by:
Total floor area:

Detached House
01 September 2020
Demi Beneke
114.94 m²

This is a Predicted Energy Assessment for a property which is not yet complete. It includes a predicted energy rating which might not represent the final energy rating of the property on completion. Once the property is completed, an Energy Performance Certificate is required providing information about the energy performance of the completed property.

Energy performance has been assessed using the SAP 2012 methodology and is rated in terms of the energy use per square metre of floor area, energy efficiency based on fuel costs and environmental impact based on carbon dioxide (CO2) emissions.



The energy efficiency rating is a measure of the overall efficiency of a home. The higher the rating the more energy efficient the home is and the lower the fuel bills are likely to be.

The environmental impact rating is a measure of a home's impact on the environment in terms of carbon dioxide (CO₂) emissions. The higher the rating the less impact it has on the environment.

SAP Input

Property Details: Land Adj 11 Queen Annes Drive

Address: Land Adj 11 Queen Annes Drive
Located in: England
Region: South England
UPRN:
Date of assessment: 01 September 2020
Date of certificate: 01 September 2020
Assessment type: New dwelling design stage
Transaction type: New dwelling
Tenure type: Unknown
Related party disclosure: No related party
Thermal Mass Parameter: Indicative Value Medium
Water use <= 125 litres/person/day: True
PCDF Version: 464

Property description:

Dwelling type: House
Detachment: Detached
Year Completed: 2020
Floor Location: **Floor area:** **Storey height:**
 Floor 0 65.15 m² 2.6 m
 Floor 1 49.79 m² 2.7 m
Living area: 32.28 m² (fraction 0.281)
Front of dwelling faces: North

Opening types:

Name:	Source:	Type:	Glazing:	Argon:	Frame:
D1	Manufacturer	Solid			PVC-U
W1	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
W2	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
W3	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
W4	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
W5	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
W6	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
W7	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
W8	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
W9	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
W10	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
W11	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
W12	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
W13	SAP 2012	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U

Name:	Gap:	Frame Factor:	g-value:	U-value:	Area:	No. of Openings:
D1	mm	0.7	0	1.8	2.3	1
W1	16mm or more	0.7	0.63	1.4	2.25	1
W2	16mm or more	0.7	0.63	1.4	0.43	1
W3	16mm or more	0.7	0.63	1.4	2.25	1
W4	16mm or more	0.7	0.63	1.4	3.49	1
W5	16mm or more	0.7	0.63	1.4	4.53	1
W6	16mm or more	0.7	0.63	1.4	6.9	1
W7	16mm or more	0.7	0.63	1.4	1.73	1
W8	16mm or more	0.7	0.63	1.4	2.25	1
W9	16mm or more	0.7	0.63	1.4	2.25	1
W10	16mm or more	0.7	0.63	1.4	2.25	1
W11	16mm or more	0.7	0.63	1.4	1.05	1

SAP Input

W12	16mm or more	0.7	0.63	1.4	1.05	1
W13	16mm or more	0.7	0.63	1.4	1.05	1

Name:	Type-Name:	Location:	Orient:	Width:	Height:
D1		External Walls	North	1	2.3
W1		External Walls	North	1.5	1.5
W2		External Walls	North	0.284	1.5
W3		External Walls	North	1.5	1.5
W4		External Walls	South	2.18	1.6
W5		External Walls	West	1.968	2.3
W6		External Walls	South	3	2.3
W7		External Walls	East	0.75	2.3
W8		External Walls	North	1.5	1.5
W9		External Walls	North	1.5	1.5
W10		External Walls	North	1.5	1.5
W11		External Walls	South	1	1.05
W12		External Walls	South	1	1.05
W13		External Walls	South	1	1.05

Overshading: Average or unknown

Opaque Elements:

Type:	Gross area:	Openings:	Net area:	U-value:	Ru value:	Curtain wall:	Kappa:
<u>External Elements</u>							
External Walls	170.96	33.78	137.18	0.19	0	False	N/A
Plain Ceiling	66.59	0	66.59	0.11	0		N/A
Ground Floor	65.15			0.17			N/A
Exposed Floor	1.44			0.22			N/A

Internal Elements

Party Elements

Thermal bridges:

Thermal bridges: User-defined (individual PSI-values) Y-Value = 0.0358

	Length	Psi-value		
	19.682	0.059	E2	Other lintels (including other steel lintels)
[Approved]	14.534	0.04	E3	Sill
[Approved]	42.9	0.05	E4	Jamb
	35.39	0.05	E5	Ground floor (normal)
	3.22	0.32	E20	Exposed floor (normal)
	3.22	0.32	E21	Exposed floor (inverted)
	20.11	0	E6	Intermediate floor within a dwelling
[Approved]	41.28	0.06	E10	Eaves (insulation at ceiling level)
	34.3	0.04	E16	Corner (normal)
	13.1	-0.052	E17	Corner (inverted internal area greater than external area)

Ventilation:

Pressure test:	Yes (As designed)
Ventilation:	Natural ventilation (extract fans)
Number of chimneys:	0
Number of open flues:	0
Number of fans:	4
Number of passive stacks:	0
Number of sides sheltered:	2
Pressure test:	5

Main heating system:

Main heating system:	Boiler systems with radiators or underfloor heating
	Gas boilers and oil boilers
	Fuel: mains gas
	Info Source: Boiler Database

SAP Input

Database: (rev 464, product index 017929) Efficiency: Winter 87.3 % Summer: 90.5
Brand name: Ideal
Model: LOGIC COMBI
Model qualifier: ESP1 35
(Combi boiler)
Systems with radiators
Central heating pump : 2013 or later
Design flow temperature: Unknown
Boiler interlock: Yes

Main heating Control:

Main heating Control: Programmer, room thermostat and TRVs
Control code: 2106

Secondary heating system:

Secondary heating system: None

Water heating:

Water heating: From main heating system
Water code: 901
Fuel :mains gas
No hot water cylinder
Solar panel: False

Others:

Electricity tariff: Standard Tariff
In Smoke Control Area: Unknown
Conservatory: No conservatory
Low energy lights: 100%
Terrain type: Low rise urban / suburban
EPC language: English
Wind turbine: No
Photovoltaics: None
Assess Zero Carbon Home: No

SAP WorkSheet: New dwelling design stage

User Details:

Assessor Name: Demi Beneke **Stroma Number:** STRO027754
Software Name: Stroma FSAP 2012 **Software Version:** Version: 1.0.4.26

Property Address: Land Adj 11 Queen Annes Drive

Address : Land Adj 11 Queen Annes Drive

1. Overall dwelling dimensions:

	Area(m ²)		Av. Height(m)		Volume(m ³)
Ground floor	65.15 (1a)	x	2.6 (2a)	=	169.39 (3a)
First floor	49.79 (1b)	x	2.7 (2b)	=	134.43 (3b)
Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n)	114.94 (4)				
Dwelling volume				(3a)+(3b)+(3c)+(3d)+(3e)+.....(3n) =	303.82 (5)

2. Ventilation rate:

	main heating	secondary heating	other	total	m ³ per hour
Number of chimneys	0	0	0	0	0 (6a)
Number of open flues	0	0	0	0	0 (6b)
Number of intermittent fans				4	40 (7a)
Number of passive vents				0	0 (7b)
Number of flueless gas fires				0	0 (7c)

Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) =	40	÷ (5) =	0.13 (8)
<i>If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)</i>			
Number of storeys in the dwelling (ns)			0 (9)
Additional infiltration		[(9)-1]x0.1 =	0 (10)
Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction			0 (11)
<i>if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35</i>			
If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0			0 (12)
If no draught lobby, enter 0.05, else enter 0			0 (13)
Percentage of windows and doors draught stripped			0 (14)
Window infiltration	0.25 - [0.2 x (14) ÷ 100] =		0 (15)
Infiltration rate	(8) + (10) + (11) + (12) + (13) + (15) =		0 (16)
Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area			5 (17)
If based on air permeability value, then (18) = [(17) ÷ 20] + (8), otherwise (18) = (16)			0.38 (18)
<i>Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used</i>			
Number of sides sheltered			2 (19)
Shelter factor	(20) = 1 - [0.075 x (19)] =		0.85 (20)
Infiltration rate incorporating shelter factor	(21) = (18) x (20) =		0.32 (21)

Infiltration rate modified for monthly wind speed

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
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Monthly average wind speed from Table 7

(22)m=	5.1	5	4.9	4.4	4.3	3.8	3.8	3.7	4	4.3	4.5	4.7
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SAP WorkSheet: New dwelling design stage

Wind Factor (22a)m = (22)m ÷ 4

(22a)m=	1.27	1.25	1.23	1.1	1.08	0.95	0.95	0.92	1	1.08	1.12	1.18
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Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

	0.41	0.41	0.4	0.36	0.35	0.31	0.31	0.3	0.32	0.35	0.36	0.38
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Calculate effective air change rate for the applicable case

If mechanical ventilation:

0 (23a)

If exhaust air heat pump using Appendix N, (23b) = (23a) × Fmv (equation (N5)) , otherwise (23b) = (23a)

0 (23b)

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

0 (23c)

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) × [1 – (23c) ÷ 100]

(24a)m= 0 0 0 0 0 0 0 0 0 0 0 0 0 (24a)

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

(24b)m= 0 0 0 0 0 0 0 0 0 0 0 0 0 (24b)

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 × (23b), then (24c) = (23b); otherwise (24c) = (22b) m + 0.5 × (23b)

(24c)m= 0 0 0 0 0 0 0 0 0 0 0 0 0 (24c)

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² x 0.5]

(24d)m= 0.59 0.58 0.58 0.56 0.56 0.55 0.55 0.55 0.55 0.56 0.57 0.57 (24d)

Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

(25)m= 0.59 0.58 0.58 0.56 0.56 0.55 0.55 0.55 0.55 0.56 0.57 0.57 (25)

3. Heat losses and heat loss parameter:

ELEMENT	Gross area (m²)	Openings m²	Net Area A ,m²	U-value W/m²K	A X U (W/K)	k-value kJ/m²·K	A X k kJ/K
Doors			2.3	x 1.8	= 4.14		(26)
Windows Type 1			2.25	x1/[1/(1.4)+ 0.04] =	2.98		(27)
Windows Type 2			0.43	x1/[1/(1.4)+ 0.04] =	0.57		(27)
Windows Type 3			2.25	x1/[1/(1.4)+ 0.04] =	2.98		(27)
Windows Type 4			3.49	x1/[1/(1.4)+ 0.04] =	4.63		(27)
Windows Type 5			4.53	x1/[1/(1.4)+ 0.04] =	6.01		(27)
Windows Type 6			6.9	x1/[1/(1.4)+ 0.04] =	9.15		(27)
Windows Type 7			1.73	x1/[1/(1.4)+ 0.04] =	2.29		(27)
Windows Type 8			2.25	x1/[1/(1.4)+ 0.04] =	2.98		(27)
Windows Type 9			2.25	x1/[1/(1.4)+ 0.04] =	2.98		(27)
Windows Type 10			2.25	x1/[1/(1.4)+ 0.04] =	2.98		(27)
Windows Type 11			1.05	x1/[1/(1.4)+ 0.04] =	1.39		(27)
Windows Type 12			1.05	x1/[1/(1.4)+ 0.04] =	1.39		(27)
Windows Type 13			1.05	x1/[1/(1.4)+ 0.04] =	1.39		(27)
Floor Type 1			65.15	x 0.17	= 11.0755		(28)
Floor Type 2			1.44	x 0.22	= 0.3168		(28)
Walls	170.96	33.78	137.18	x 0.19	= 26.06		(29)

SAP WorkSheet: New dwelling design stage

Roof

 x

 =

 (30)

Total area of elements, m²

 (31)

* for windows and roof windows, use effective window U-value calculated using formula $1/[(1/U\text{-value})+0.04]$ as given in paragraph 3.2

** include the areas on both sides of internal walls and partitions

Fabric heat loss, W/K = S (A x U) (26)...(30) + (32) =

 (33)

Heat capacity Cm = S(A x k) ((28)...(30) + (32) + (32a)...(32e) =

 (34)

Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m²K Indicative Value: Medium

 (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f can be used instead of a detailed calculation.

Thermal bridges : S (L x Y) calculated using Appendix K

 (36)

if details of thermal bridging are not known (36) = 0.05 x (31)

Total fabric heat loss (33) + (36) =

 (37)

Ventilation heat loss calculated monthly (38)m = 0.33 x (25)m x (5)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(38)m=	58.71	58.37	58.05	56.51	56.23	54.89	54.89	54.64	55.41	56.23	56.81	57.41	(38)

Heat transfer coefficient, W/K (39)m = (37) + (38)m

(39)m=	160.25	159.92	159.59	158.06	157.77	156.43	156.43	156.19	156.95	157.77	158.35	158.96	
	Average = Sum(39) _{1...12} /12=											<table border="1" style="display: inline-table; width: 80px; text-align: center;">158.05</table>	(39)

Heat loss parameter (HLP), W/m²K (40)m = (39)m ÷ (4)

(40)m=	1.39	1.39	1.39	1.38	1.37	1.36	1.36	1.36	1.37	1.37	1.38	1.38	
	Average = Sum(40) _{1...12} /12=											<table border="1" style="display: inline-table; width: 80px; text-align: center;">1.38</table>	(40)

Number of days in month (Table 1a)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(41)m=	31	28	31	30	31	30	31	31	30	31	30	31	(41)

4. Water heating energy requirement: kWh/year:

Assumed occupancy, N

 (42)

if TFA > 13.9, N = 1 + 1.76 x [1 - exp(-0.000349 x (TFA -13.9)²)] + 0.0013 x (TFA -13.9)

if TFA ≤ 13.9, N = 1

Annual average hot water usage in litres per day Vd,average = (25 x N) + 36

 (43)

Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(44)m=	111.85	107.79	103.72	99.65	95.58	91.52	91.52	95.58	99.65	103.72	107.79	111.85	
	Total = Sum(44) _{1...12} =											<table border="1" style="display: inline-table; width: 80px; text-align: center;">1220.21</table>	(44)

Energy content of hot water used - calculated monthly = 4.190 x Vd,m x nm x DTm / 3600 kWh/month (see Tables 1b, 1c, 1d)

(45)m=	165.87	145.07	149.7	130.52	125.23	108.07	100.14	114.91	116.28	135.52	147.93	160.64	
	Total = Sum(45) _{1...12} =											<table border="1" style="display: inline-table; width: 80px; text-align: center;">1599.89</table>	(45)

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

(46)m=	24.88	21.76	22.46	19.58	18.78	16.21	15.02	17.24	17.44	20.33	22.19	24.1	(46)
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Water storage loss:

Storage volume (litres) including any solar or WWHRS storage within same vessel

 (47)

If community heating and no tank in dwelling, enter 110 litres in (47)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in (47)

Water storage loss:

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a) If manufacturer's declared loss factor is known (kWh/day): 0 (48)

Temperature factor from Table 2b 0 (49)

Energy lost from water storage, kWh/year (48) x (49) = 0 (50)

b) If manufacturer's declared cylinder loss factor is not known:

Hot water storage loss factor from Table 2 (kWh/litre/day) 0 (51)

If community heating see section 4.3

Volume factor from Table 2a 0 (52)

Temperature factor from Table 2b 0 (53)

Energy lost from water storage, kWh/year (47) x (51) x (52) x (53) = 0 (54)

Enter (50) or (54) in (55) 0 (55)

Water storage loss calculated for each month ((56)m = (55) x (41)m

(56)m=

0	0	0	0	0	0	0	0	0	0	0	0
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(56)

If cylinder contains dedicated solar storage, (57)m = (56)m x [(50) - (H11)] ÷ (50), else (57)m = (56)m where (H11) is from Appendix H

(57)m=

0	0	0	0	0	0	0	0	0	0	0	0
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(57)

Primary circuit loss (annual) from Table 3 0 (58)

Primary circuit loss calculated for each month (59)m = (58) ÷ 365 x (41)m

(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat)

(59)m=

0	0	0	0	0	0	0	0	0	0	0	0
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(59)

Combi loss calculated for each month (61)m = (60) ÷ 365 x (41)m

(61)m=

14.15	12.77	14.12	13.62	14.04	13.55	13.98	14.02	13.59	14.08	13.67	14.14
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(61)

Total heat required for water heating calculated for each month (62)m = 0.85 x (45)m + (46)m + (57)m + (59)m + (61)m

(62)m=

180.03	157.85	163.82	144.14	139.28	121.62	114.12	128.93	129.87	149.6	161.6	174.78
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(62)

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)

(add additional lines if FGHRs and/or WWHRs applies, see Appendix G)

(63)m=

0	0	0	0	0	0	0	0	0	0	0	0
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(63)

Output from water heater

(64)m=

180.03	157.85	163.82	144.14	139.28	121.62	114.12	128.93	129.87	149.6	161.6	174.78
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Output from water heater (annual)_{1...12} 1765.63 (64)

Heat gains from water heating, kWh/month $0.25 \times [0.85 \times (45)m + (61)m] + 0.8 \times [(46)m + (57)m + (59)m]$

(65)m=

58.69	51.43	53.31	46.8	45.15	39.32	36.79	41.71	42.06	48.58	52.6	56.95
-------	-------	-------	------	-------	-------	-------	-------	-------	-------	------	-------

(65)

include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts

(66)m=

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
170.49	170.49	170.49	170.49	170.49	170.49	170.49	170.49	170.49	170.49	170.49	170.49

(66)

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5

(67)m=

62.06	55.13	44.83	33.94	25.37	21.42	23.14	30.08	40.38	51.27	59.84	63.79
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

(67)

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5

(68)m=

415.63	419.94	409.07	385.94	356.73	329.28	310.94	306.63	317.49	340.63	369.84	397.29
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

(68)

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5

(69)m=

54.89	54.89	54.89	54.89	54.89	54.89	54.89	54.89	54.89	54.89	54.89	54.89
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

(69)

Pumps and fans gains (Table 5a)

(70)m=

3	3	3	3	3	3	3	3	3	3	3	3
---	---	---	---	---	---	---	---	---	---	---	---

(70)

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Losses e.g. evaporation (negative values) (Table 5)

(71)m=

-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66
---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------

 (71)

Water heating gains (Table 5)

(72)m=

78.89	76.53	71.65	65	60.69	54.61	49.45	56.07	58.42	65.3	73.06	76.54
-------	-------	-------	----	-------	-------	-------	-------	-------	------	-------	-------

 (72)

Total internal gains = (66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m

(73)m=

671.3	666.32	640.27	599.6	557.5	520.03	498.25	507.49	531.01	571.92	617.46	652.34
-------	--------	--------	-------	-------	--------	--------	--------	--------	--------	--------	--------

 (73)

6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

Orientation:	Access Factor Table 6d		Area m ²		Flux Table 6a		g_ Table 6b		FF Table 6c		Gains (W)							
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>7.31</td></tr></table> (74)	7.31
0.77																		
2.25																		
10.63																		
0.63																		
0.7																		
7.31																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.43</td></tr></table>	0.43	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>1.4</td></tr></table> (74)	1.4
0.77																		
0.43																		
10.63																		
0.63																		
0.7																		
1.4																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>7.31</td></tr></table> (74)	7.31
0.77																		
2.25																		
10.63																		
0.63																		
0.7																		
7.31																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>7.31</td></tr></table> (74)	7.31
0.77																		
2.25																		
10.63																		
0.63																		
0.7																		
7.31																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>7.31</td></tr></table> (74)	7.31
0.77																		
2.25																		
10.63																		
0.63																		
0.7																		
7.31																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>7.31</td></tr></table> (74)	7.31
0.77																		
2.25																		
10.63																		
0.63																		
0.7																		
7.31																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>13.97</td></tr></table> (74)	13.97
0.77																		
2.25																		
20.32																		
0.63																		
0.7																		
13.97																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.43</td></tr></table>	0.43	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>2.67</td></tr></table> (74)	2.67
0.77																		
0.43																		
20.32																		
0.63																		
0.7																		
2.67																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>13.97</td></tr></table> (74)	13.97
0.77																		
2.25																		
20.32																		
0.63																		
0.7																		
13.97																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>13.97</td></tr></table> (74)	13.97
0.77																		
2.25																		
20.32																		
0.63																		
0.7																		
13.97																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>13.97</td></tr></table> (74)	13.97
0.77																		
2.25																		
20.32																		
0.63																		
0.7																		
13.97																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>13.97</td></tr></table> (74)	13.97
0.77																		
2.25																		
20.32																		
0.63																		
0.7																		
13.97																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>23.74</td></tr></table> (74)	23.74
0.77																		
2.25																		
34.53																		
0.63																		
0.7																		
23.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.43</td></tr></table>	0.43	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>4.54</td></tr></table> (74)	4.54
0.77																		
0.43																		
34.53																		
0.63																		
0.7																		
4.54																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>23.74</td></tr></table> (74)	23.74
0.77																		
2.25																		
34.53																		
0.63																		
0.7																		
23.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>23.74</td></tr></table> (74)	23.74
0.77																		
2.25																		
34.53																		
0.63																		
0.7																		
23.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>23.74</td></tr></table> (74)	23.74
0.77																		
2.25																		
34.53																		
0.63																		
0.7																		
23.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>23.74</td></tr></table> (74)	23.74
0.77																		
2.25																		
34.53																		
0.63																		
0.7																		
23.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>38.14</td></tr></table> (74)	38.14
0.77																		
2.25																		
55.46																		
0.63																		
0.7																		
38.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.43</td></tr></table>	0.43	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>7.29</td></tr></table> (74)	7.29
0.77																		
0.43																		
55.46																		
0.63																		
0.7																		
7.29																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>38.14</td></tr></table> (74)	38.14
0.77																		
2.25																		
55.46																		
0.63																		
0.7																		
38.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>38.14</td></tr></table> (74)	38.14
0.77																		
2.25																		
55.46																		
0.63																		
0.7																		
38.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>38.14</td></tr></table> (74)	38.14
0.77																		
2.25																		
55.46																		
0.63																		
0.7																		
38.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>38.14</td></tr></table> (74)	38.14
0.77																		
2.25																		
55.46																		
0.63																		
0.7																		
38.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>51.38</td></tr></table> (74)	51.38
0.77																		
2.25																		
74.72																		
0.63																		
0.7																		
51.38																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.43</td></tr></table>	0.43	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>9.82</td></tr></table> (74)	9.82
0.77																		
0.43																		
74.72																		
0.63																		
0.7																		
9.82																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>51.38</td></tr></table> (74)	51.38
0.77																		
2.25																		
74.72																		
0.63																		
0.7																		
51.38																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>51.38</td></tr></table> (74)	51.38
0.77																		
2.25																		
74.72																		
0.63																		
0.7																		
51.38																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>51.38</td></tr></table> (74)	51.38
0.77																		
2.25																		
74.72																		
0.63																		
0.7																		
51.38																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>51.38</td></tr></table> (74)	51.38
0.77																		
2.25																		
74.72																		
0.63																		
0.7																		
51.38																		

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North	0.9x	0.77	x	2.25	x	79.99	x	0.63	x	0.7	=	55	(74)
North	0.9x	0.77	x	0.43	x	79.99	x	0.63	x	0.7	=	10.51	(74)
North	0.9x	0.77	x	2.25	x	79.99	x	0.63	x	0.7	=	55	(74)
North	0.9x	0.77	x	2.25	x	79.99	x	0.63	x	0.7	=	55	(74)
North	0.9x	0.77	x	2.25	x	79.99	x	0.63	x	0.7	=	55	(74)
North	0.9x	0.77	x	2.25	x	79.99	x	0.63	x	0.7	=	55	(74)
North	0.9x	0.77	x	2.25	x	74.68	x	0.63	x	0.7	=	51.35	(74)
North	0.9x	0.77	x	0.43	x	74.68	x	0.63	x	0.7	=	9.81	(74)
North	0.9x	0.77	x	2.25	x	74.68	x	0.63	x	0.7	=	51.35	(74)
North	0.9x	0.77	x	2.25	x	74.68	x	0.63	x	0.7	=	51.35	(74)
North	0.9x	0.77	x	2.25	x	74.68	x	0.63	x	0.7	=	51.35	(74)
North	0.9x	0.77	x	2.25	x	74.68	x	0.63	x	0.7	=	51.35	(74)
North	0.9x	0.77	x	2.25	x	59.25	x	0.63	x	0.7	=	40.74	(74)
North	0.9x	0.77	x	0.43	x	59.25	x	0.63	x	0.7	=	7.79	(74)
North	0.9x	0.77	x	2.25	x	59.25	x	0.63	x	0.7	=	40.74	(74)
North	0.9x	0.77	x	2.25	x	59.25	x	0.63	x	0.7	=	40.74	(74)
North	0.9x	0.77	x	2.25	x	59.25	x	0.63	x	0.7	=	40.74	(74)
North	0.9x	0.77	x	2.25	x	59.25	x	0.63	x	0.7	=	40.74	(74)
North	0.9x	0.77	x	2.25	x	41.52	x	0.63	x	0.7	=	28.55	(74)
North	0.9x	0.77	x	0.43	x	41.52	x	0.63	x	0.7	=	5.46	(74)
North	0.9x	0.77	x	2.25	x	41.52	x	0.63	x	0.7	=	28.55	(74)
North	0.9x	0.77	x	2.25	x	41.52	x	0.63	x	0.7	=	28.55	(74)
North	0.9x	0.77	x	2.25	x	41.52	x	0.63	x	0.7	=	28.55	(74)
North	0.9x	0.77	x	2.25	x	41.52	x	0.63	x	0.7	=	28.55	(74)
North	0.9x	0.77	x	2.25	x	24.19	x	0.63	x	0.7	=	16.63	(74)
North	0.9x	0.77	x	0.43	x	24.19	x	0.63	x	0.7	=	3.18	(74)
North	0.9x	0.77	x	2.25	x	24.19	x	0.63	x	0.7	=	16.63	(74)
North	0.9x	0.77	x	2.25	x	24.19	x	0.63	x	0.7	=	16.63	(74)
North	0.9x	0.77	x	2.25	x	24.19	x	0.63	x	0.7	=	16.63	(74)
North	0.9x	0.77	x	2.25	x	24.19	x	0.63	x	0.7	=	16.63	(74)
North	0.9x	0.77	x	2.25	x	13.12	x	0.63	x	0.7	=	9.02	(74)
North	0.9x	0.77	x	0.43	x	13.12	x	0.63	x	0.7	=	1.72	(74)
North	0.9x	0.77	x	2.25	x	13.12	x	0.63	x	0.7	=	9.02	(74)
North	0.9x	0.77	x	2.25	x	13.12	x	0.63	x	0.7	=	9.02	(74)
North	0.9x	0.77	x	2.25	x	13.12	x	0.63	x	0.7	=	9.02	(74)
North	0.9x	0.77	x	2.25	x	8.86	x	0.63	x	0.7	=	6.1	(74)
North	0.9x	0.77	x	0.43	x	8.86	x	0.63	x	0.7	=	1.16	(74)
North	0.9x	0.77	x	2.25	x	8.86	x	0.63	x	0.7	=	6.1	(74)
North	0.9x	0.77	x	2.25	x	8.86	x	0.63	x	0.7	=	6.1	(74)
North	0.9x	0.77	x	2.25	x	8.86	x	0.63	x	0.7	=	6.1	(74)

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North	0.9x	0.77	x	2.25	x	8.86	x	0.63	x	0.7	=	6.1	(74)
East	0.9x	0.77	x	1.73	x	19.64	x	0.63	x	0.7	=	10.38	(76)
East	0.9x	0.77	x	1.73	x	38.42	x	0.63	x	0.7	=	20.31	(76)
East	0.9x	0.77	x	1.73	x	63.27	x	0.63	x	0.7	=	33.45	(76)
East	0.9x	0.77	x	1.73	x	92.28	x	0.63	x	0.7	=	48.79	(76)
East	0.9x	0.77	x	1.73	x	113.09	x	0.63	x	0.7	=	59.79	(76)
East	0.9x	0.77	x	1.73	x	115.77	x	0.63	x	0.7	=	61.21	(76)
East	0.9x	0.77	x	1.73	x	110.22	x	0.63	x	0.7	=	58.27	(76)
East	0.9x	0.77	x	1.73	x	94.68	x	0.63	x	0.7	=	50.06	(76)
East	0.9x	0.77	x	1.73	x	73.59	x	0.63	x	0.7	=	38.91	(76)
East	0.9x	0.77	x	1.73	x	45.59	x	0.63	x	0.7	=	24.1	(76)
East	0.9x	0.77	x	1.73	x	24.49	x	0.63	x	0.7	=	12.95	(76)
East	0.9x	0.77	x	1.73	x	16.15	x	0.63	x	0.7	=	8.54	(76)
South	0.9x	0.77	x	3.49	x	46.75	x	0.63	x	0.7	=	49.87	(78)
South	0.9x	0.77	x	6.9	x	46.75	x	0.63	x	0.7	=	98.59	(78)
South	0.9x	0.77	x	1.05	x	46.75	x	0.63	x	0.7	=	15	(78)
South	0.9x	0.77	x	1.05	x	46.75	x	0.63	x	0.7	=	15	(78)
South	0.9x	0.77	x	1.05	x	46.75	x	0.63	x	0.7	=	15	(78)
South	0.9x	0.77	x	3.49	x	76.57	x	0.63	x	0.7	=	81.67	(78)
South	0.9x	0.77	x	6.9	x	76.57	x	0.63	x	0.7	=	161.46	(78)
South	0.9x	0.77	x	1.05	x	76.57	x	0.63	x	0.7	=	24.57	(78)
South	0.9x	0.77	x	1.05	x	76.57	x	0.63	x	0.7	=	24.57	(78)
South	0.9x	0.77	x	1.05	x	76.57	x	0.63	x	0.7	=	24.57	(78)
South	0.9x	0.77	x	3.49	x	97.53	x	0.63	x	0.7	=	104.03	(78)
South	0.9x	0.77	x	6.9	x	97.53	x	0.63	x	0.7	=	205.67	(78)
South	0.9x	0.77	x	1.05	x	97.53	x	0.63	x	0.7	=	31.3	(78)
South	0.9x	0.77	x	1.05	x	97.53	x	0.63	x	0.7	=	31.3	(78)
South	0.9x	0.77	x	1.05	x	97.53	x	0.63	x	0.7	=	31.3	(78)
South	0.9x	0.77	x	3.49	x	110.23	x	0.63	x	0.7	=	117.57	(78)
South	0.9x	0.77	x	6.9	x	110.23	x	0.63	x	0.7	=	232.45	(78)
South	0.9x	0.77	x	1.05	x	110.23	x	0.63	x	0.7	=	35.37	(78)
South	0.9x	0.77	x	1.05	x	110.23	x	0.63	x	0.7	=	35.37	(78)
South	0.9x	0.77	x	1.05	x	110.23	x	0.63	x	0.7	=	35.37	(78)
South	0.9x	0.77	x	3.49	x	114.87	x	0.63	x	0.7	=	122.52	(78)
South	0.9x	0.77	x	6.9	x	114.87	x	0.63	x	0.7	=	242.23	(78)
South	0.9x	0.77	x	1.05	x	114.87	x	0.63	x	0.7	=	36.86	(78)
South	0.9x	0.77	x	1.05	x	114.87	x	0.63	x	0.7	=	36.86	(78)
South	0.9x	0.77	x	1.05	x	114.87	x	0.63	x	0.7	=	36.86	(78)
South	0.9x	0.77	x	3.49	x	110.55	x	0.63	x	0.7	=	117.91	(78)
South	0.9x	0.77	x	6.9	x	110.55	x	0.63	x	0.7	=	233.12	(78)
South	0.9x	0.77	x	1.05	x	110.55	x	0.63	x	0.7	=	35.47	(78)

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South	0.9x	0.77	x	1.05	x	110.55	x	0.63	x	0.7	=	35.47	(78)
South	0.9x	0.77	x	1.05	x	110.55	x	0.63	x	0.7	=	35.47	(78)
South	0.9x	0.77	x	3.49	x	108.01	x	0.63	x	0.7	=	115.2	(78)
South	0.9x	0.77	x	6.9	x	108.01	x	0.63	x	0.7	=	227.77	(78)
South	0.9x	0.77	x	1.05	x	108.01	x	0.63	x	0.7	=	34.66	(78)
South	0.9x	0.77	x	1.05	x	108.01	x	0.63	x	0.7	=	34.66	(78)
South	0.9x	0.77	x	1.05	x	108.01	x	0.63	x	0.7	=	34.66	(78)
South	0.9x	0.77	x	3.49	x	104.89	x	0.63	x	0.7	=	111.88	(78)
South	0.9x	0.77	x	6.9	x	104.89	x	0.63	x	0.7	=	221.19	(78)
South	0.9x	0.77	x	1.05	x	104.89	x	0.63	x	0.7	=	33.66	(78)
South	0.9x	0.77	x	1.05	x	104.89	x	0.63	x	0.7	=	33.66	(78)
South	0.9x	0.77	x	1.05	x	104.89	x	0.63	x	0.7	=	33.66	(78)
South	0.9x	0.77	x	3.49	x	101.89	x	0.63	x	0.7	=	108.67	(78)
South	0.9x	0.77	x	6.9	x	101.89	x	0.63	x	0.7	=	214.85	(78)
South	0.9x	0.77	x	1.05	x	101.89	x	0.63	x	0.7	=	32.69	(78)
South	0.9x	0.77	x	1.05	x	101.89	x	0.63	x	0.7	=	32.69	(78)
South	0.9x	0.77	x	1.05	x	101.89	x	0.63	x	0.7	=	32.69	(78)
South	0.9x	0.77	x	3.49	x	82.59	x	0.63	x	0.7	=	88.08	(78)
South	0.9x	0.77	x	6.9	x	82.59	x	0.63	x	0.7	=	174.15	(78)
South	0.9x	0.77	x	1.05	x	82.59	x	0.63	x	0.7	=	26.5	(78)
South	0.9x	0.77	x	1.05	x	82.59	x	0.63	x	0.7	=	26.5	(78)
South	0.9x	0.77	x	1.05	x	82.59	x	0.63	x	0.7	=	26.5	(78)
South	0.9x	0.77	x	3.49	x	55.42	x	0.63	x	0.7	=	59.11	(78)
South	0.9x	0.77	x	6.9	x	55.42	x	0.63	x	0.7	=	116.86	(78)
South	0.9x	0.77	x	1.05	x	55.42	x	0.63	x	0.7	=	17.78	(78)
South	0.9x	0.77	x	1.05	x	55.42	x	0.63	x	0.7	=	17.78	(78)
South	0.9x	0.77	x	1.05	x	55.42	x	0.63	x	0.7	=	17.78	(78)
South	0.9x	0.77	x	3.49	x	40.4	x	0.63	x	0.7	=	43.09	(78)
South	0.9x	0.77	x	6.9	x	40.4	x	0.63	x	0.7	=	85.19	(78)
South	0.9x	0.77	x	1.05	x	40.4	x	0.63	x	0.7	=	12.96	(78)
South	0.9x	0.77	x	1.05	x	40.4	x	0.63	x	0.7	=	12.96	(78)
South	0.9x	0.77	x	1.05	x	40.4	x	0.63	x	0.7	=	12.96	(78)
West	0.9x	0.77	x	4.53	x	19.64	x	0.63	x	0.7	=	27.19	(80)
West	0.9x	0.77	x	4.53	x	38.42	x	0.63	x	0.7	=	53.19	(80)
West	0.9x	0.77	x	4.53	x	63.27	x	0.63	x	0.7	=	87.6	(80)
West	0.9x	0.77	x	4.53	x	92.28	x	0.63	x	0.7	=	127.76	(80)
West	0.9x	0.77	x	4.53	x	113.09	x	0.63	x	0.7	=	156.57	(80)
West	0.9x	0.77	x	4.53	x	115.77	x	0.63	x	0.7	=	160.28	(80)
West	0.9x	0.77	x	4.53	x	110.22	x	0.63	x	0.7	=	152.59	(80)
West	0.9x	0.77	x	4.53	x	94.68	x	0.63	x	0.7	=	131.07	(80)
West	0.9x	0.77	x	4.53	x	73.59	x	0.63	x	0.7	=	101.88	(80)

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West	0.9x	0.77	x	4.53	x	45.59	x	0.63	x	0.7	=	63.11	(80)
West	0.9x	0.77	x	4.53	x	24.49	x	0.63	x	0.7	=	33.9	(80)
West	0.9x	0.77	x	4.53	x	16.15	x	0.63	x	0.7	=	22.36	(80)

Solar gains in watts, calculated for each month

(83)m = Sum(74)m ... (82)m

(83)m=	268.99	462.88	647.9	830.68	958.4	964.44	924.38	826.66	710.58	515.3	322.99	229.71	(83)
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Total gains – internal and solar (84)m = (73)m + (83)m , watts

(84)m=	940.29	1129.2	1288.17	1430.28	1515.91	1484.47	1422.63	1334.16	1241.6	1087.22	940.45	882.05	(84)
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7. Mean internal temperature (heating season)

Temperature during heating periods in the living area from Table 9, Th1 (°C)

21 (85)

Utilisation factor for gains for living area, h1,m (see Table 9a)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(86)m=	0.99	0.98	0.96	0.91	0.8	0.63	0.47	0.52	0.75	0.94	0.99	0.99	(86)

Mean internal temperature in living area T1 (follow steps 3 to 7 in Table 9c)

(87)m=	19.64	19.85	20.16	20.52	20.8	20.95	20.99	20.98	20.89	20.51	20	19.59	(87)
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Temperature during heating periods in rest of dwelling from Table 9, Th2 (°C)

(88)m=	19.77	19.77	19.77	19.78	19.78	19.79	19.79	19.8	19.79	19.78	19.78	19.78	(88)
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Utilisation factor for gains for rest of dwelling, h2,m (see Table 9a)

(89)m=	0.99	0.98	0.95	0.88	0.74	0.53	0.35	0.39	0.66	0.91	0.98	0.99	(89)
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Mean internal temperature in the rest of dwelling T2 (follow steps 3 to 7 in Table 9c)

(90)m=	18.56	18.77	19.07	19.42	19.66	19.77	19.79	19.79	19.73	19.42	18.93	18.52	(90)
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fLA = Living area ÷ (4) =

0.28 (91)

Mean internal temperature (for the whole dwelling) = fLA × T1 + (1 – fLA) × T2

(92)m=	18.86	19.08	19.38	19.73	19.98	20.1	20.13	20.13	20.06	19.73	19.23	18.82	(92)
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Apply adjustment to the mean internal temperature from Table 4e, where appropriate

(93)m=	18.86	19.08	19.38	19.73	19.98	20.1	20.13	20.13	20.06	19.73	19.23	18.82	(93)
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8. Space heating requirement

Set Ti to the mean internal temperature obtained at step 11 of Table 9b, so that Ti,m=(76)m and re-calculate the utilisation factor for gains using Table 9a

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
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Utilisation factor for gains, hm:

(94)m=	0.99	0.97	0.95	0.88	0.75	0.56	0.38	0.43	0.68	0.91	0.98	0.99	(94)
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Useful gains, hmGm , W = (94)m x (84)m

(95)m=	929.14	1100.75	1218.98	1256.77	1135.23	826.11	546.5	573.29	850.14	987.22	918.65	873.9	(95)
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Monthly average external temperature from Table 8

(96)m=	4.3	4.9	6.5	8.9	11.7	14.6	16.6	16.4	14.1	10.6	7.1	4.2	(96)
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Heat loss rate for mean internal temperature, Lm , W =[(39)m x [(93)m– (96)m]

(97)m=	2333.31	2267.17	2055.23	1711.67	1306.48	860.78	551.76	581.85	935.01	1440.25	1920.7	2324.45	(97)
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Space heating requirement for each month, kWh/month = 0.024 x [(97)m – (95)m] x (41)m

(98)m=	1044.7	783.84	622.17	327.53	127.41	0	0	0	0	337.06	721.48	1079.21	(98)
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Total per year (kWh/year) = Sum(98)1...5,9...12 =

5043.39 (98)

Space heating requirement in kWh/m²/year

43.88 (99)

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9a. Energy requirements – Individual heating systems including micro-CHP)

Space heating:

Fraction of space heat from secondary/supplementary system		0	(201)
Fraction of space heat from main system(s)	(202) = 1 – (201) =	1	(202)
Fraction of total heating from main system 1	(204) = (202) × [1 – (203)] =	1	(204)
Efficiency of main space heating system 1		90.5	(206)
Efficiency of secondary/supplementary heating system, %		0	(208)

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	kWh/year
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Space heating requirement (calculated above)

1044.7	783.84	622.17	327.53	127.41	0	0	0	0	337.06	721.48	1079.21	
(211)m = {[[(98)m x (204)] } x 100 ÷ (206)												(211)
1154.36	866.12	687.48	361.91	140.79	0	0	0	0	372.44	797.21	1192.5	
Total (kWh/year) =Sum(211) _{1...5,10...12} =												5572.81 (211)

Space heating fuel (secondary), kWh/month

= {[[(98)m x (201)] } x 100 ÷ (208)

(215)m=	0	0	0	0	0	0	0	0	0	0	0	
Total (kWh/year) =Sum(215) _{1...5,10...12} =												0 (215)

Water heating

Output from water heater (calculated above)

180.03	157.85	163.82	144.14	139.28	121.62	114.12	128.93	129.87	149.6	161.6	174.78	
Efficiency of water heater												87.3 (216)
(217)m=	90.01	89.95	89.81	89.5	88.8	87.3	87.3	87.3	87.3	89.49	89.9	90.04 (217)

Fuel for water heating, kWh/month

(219)m = (64)m x 100 ÷ (217)m

(219)m=	200	175.49	182.4	161.06	156.84	139.31	130.72	147.69	148.77	167.17	179.76	194.12
Total = Sum(219a) _{1...12} =												1983.31 (219)

Annual totals

	kWh/year	kWh/year
Space heating fuel used, main system 1		5572.81
Water heating fuel used		1983.31

Electricity for pumps, fans and electric keep-hot

central heating pump:	30	(230c)
boiler with a fan-assisted flue	45	(230e)
Total electricity for the above, kWh/year	sum of (230a)...(230g) =	75 (231)
Electricity for lighting		438.43 (232)

10a. Fuel costs - individual heating systems:

	Fuel kWh/year	Fuel Price (Table 12)	Fuel Cost £/year
Space heating - main system 1	(211) x	3.48	x 0.01 = 193.93 (240)
Space heating - main system 2	(213) x	0	x 0.01 = 0 (241)
Space heating - secondary	(215) x	13.19	x 0.01 = 0 (242)
Water heating cost (other fuel)	(219)	3.48	x 0.01 = 69.02 (247)

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Pumps, fans and electric keep-hot	(231)	13.19	x 0.01 =	9.89	(249)
(if off-peak tariff, list each of (230a) to (230g) separately as applicable and apply fuel price according to Table 12a)					
Energy for lighting	(232)	13.19	x 0.01 =	57.83	(250)
Additional standing charges (Table 12)				120	(251)
Appendix Q items: repeat lines (253) and (254) as needed					
Total energy cost	(245)...(247) + (250)...(254) =			450.67	(255)

11a. SAP rating - individual heating systems

Energy cost deflator (Table 12)		0.42	(256)
Energy cost factor (ECF)	[(255) x (256)] ÷ [(4) + 45.0] =	1.18	(257)
SAP rating (Section 12)		83.49	(258)

12a. CO2 emissions – Individual heating systems including micro-CHP

	Energy kWh/year	Emission factor kg CO2/kWh	Emissions kg CO2/year
Space heating (main system 1)	(211) x	0.216	= 1203.73 (261)
Space heating (secondary)	(215) x	0.519	= 0 (263)
Water heating	(219) x	0.216	= 428.4 (264)
Space and water heating	(261) + (262) + (263) + (264) =		1632.12 (265)
Electricity for pumps, fans and electric keep-hot	(231) x	0.519	= 38.93 (267)
Electricity for lighting	(232) x	0.519	= 227.55 (268)
Total CO2, kg/year		sum of (265)...(271) =	1898.59 (272)
CO2 emissions per m²		(272) ÷ (4) =	16.52 (273)
El rating (section 14)			84 (274)

13a. Primary Energy

	Energy kWh/year	Primary factor	P. Energy kWh/year
Space heating (main system 1)	(211) x	1.22	= 6798.83 (261)
Space heating (secondary)	(215) x	3.07	= 0 (263)
Energy for water heating	(219) x	1.22	= 2419.64 (264)
Space and water heating	(261) + (262) + (263) + (264) =		9218.47 (265)
Electricity for pumps, fans and electric keep-hot	(231) x	3.07	= 230.25 (267)
Electricity for lighting	(232) x	0	= 1345.99 (268)
'Total Primary Energy		sum of (265)...(271) =	10794.71 (272)
Primary energy kWh/m²/year		(272) ÷ (4) =	93.92 (273)

DER WorkSheet: New dwelling design stage

User Details:

Assessor Name: Demi Beneke **Stroma Number:** STRO027754
Software Name: Stroma FSAP 2012 **Software Version:** Version: 1.0.4.26

Property Address: Land Adj 11 Queen Annes Drive

Address : Land Adj 11 Queen Annes Drive

1. Overall dwelling dimensions:

	Area(m ²)		Av. Height(m)		Volume(m ³)
Ground floor	65.15 (1a)	x	2.6 (2a)	=	169.39 (3a)
First floor	49.79 (1b)	x	2.7 (2b)	=	134.43 (3b)
Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n)	114.94 (4)				
Dwelling volume				(3a)+(3b)+(3c)+(3d)+(3e)+.....(3n) =	303.82 (5)

2. Ventilation rate:

	main heating	secondary heating	other	total	m ³ per hour
Number of chimneys	0	0	0	0	0 (6a)
Number of open flues	0	0	0	0	0 (6b)
Number of intermittent fans				4	40 (7a)
Number of passive vents				0	0 (7b)
Number of flueless gas fires				0	0 (7c)

Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) =	40	÷ (5) =	0.13 (8)
<i>If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)</i>			
Number of storeys in the dwelling (ns)			0 (9)
Additional infiltration		[(9)-1]x0.1 =	0 (10)
Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction			0 (11)
<i>if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35</i>			
If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0			0 (12)
If no draught lobby, enter 0.05, else enter 0			0 (13)
Percentage of windows and doors draught stripped			0 (14)
Window infiltration	0.25 - [0.2 x (14) ÷ 100] =		0 (15)
Infiltration rate	(8) + (10) + (11) + (12) + (13) + (15) =		0 (16)
Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area			5 (17)
If based on air permeability value, then (18) = [(17) ÷ 20] + (8), otherwise (18) = (16)			0.38 (18)
<i>Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used</i>			
Number of sides sheltered			2 (19)
Shelter factor	(20) = 1 - [0.075 x (19)] =		0.85 (20)
Infiltration rate incorporating shelter factor	(21) = (18) x (20) =		0.32 (21)

Infiltration rate modified for monthly wind speed

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

Monthly average wind speed from Table 7

(22)m=	5.1	5	4.9	4.4	4.3	3.8	3.8	3.7	4	4.3	4.5	4.7
--------	-----	---	-----	-----	-----	-----	-----	-----	---	-----	-----	-----

DER WorkSheet: New dwelling design stage

Wind Factor (22a)m = (22)m ÷ 4

(22a)m=	1.27	1.25	1.23	1.1	1.08	0.95	0.95	0.92	1	1.08	1.12	1.18
---------	------	------	------	-----	------	------	------	------	---	------	------	------

Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

	0.41	0.41	0.4	0.36	0.35	0.31	0.31	0.3	0.32	0.35	0.36	0.38
--	------	------	-----	------	------	------	------	-----	------	------	------	------

Calculate effective air change rate for the applicable case

If mechanical ventilation:

0 (23a)

If exhaust air heat pump using Appendix N, (23b) = (23a) × Fmv (equation (N5)) , otherwise (23b) = (23a)

0 (23b)

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

0 (23c)

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) × [1 – (23c) ÷ 100]

(24a)m=	0	0	0	0	0	0	0	0	0	0	0	0	(24a)
---------	---	---	---	---	---	---	---	---	---	---	---	---	-------

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

(24b)m=	0	0	0	0	0	0	0	0	0	0	0	0	(24b)
---------	---	---	---	---	---	---	---	---	---	---	---	---	-------

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 × (23b), then (24c) = (23b); otherwise (24c) = (22b) m + 0.5 × (23b)

(24c)m=	0	0	0	0	0	0	0	0	0	0	0	0	(24c)
---------	---	---	---	---	---	---	---	---	---	---	---	---	-------

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² x 0.5]

(24d)m=	0.59	0.58	0.58	0.56	0.56	0.55	0.55	0.55	0.55	0.56	0.57	0.57	(24d)
---------	------	------	------	------	------	------	------	------	------	------	------	------	-------

Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

(25)m=	0.59	0.58	0.58	0.56	0.56	0.55	0.55	0.55	0.55	0.56	0.57	0.57	(25)
--------	------	------	------	------	------	------	------	------	------	------	------	------	------

3. Heat losses and heat loss parameter:

ELEMENT	Gross area (m²)	Openings m²	Net Area A ,m²	U-value W/m²K	A X U (W/K)	k-value kJ/m²·K	A X k kJ/K
Doors			2.3	x 1.8	= 4.14		(26)
Windows Type 1			2.25	x 1/[1/(1.4)+ 0.04]	= 2.98		(27)
Windows Type 2			0.43	x 1/[1/(1.4)+ 0.04]	= 0.57		(27)
Windows Type 3			2.25	x 1/[1/(1.4)+ 0.04]	= 2.98		(27)
Windows Type 4			3.49	x 1/[1/(1.4)+ 0.04]	= 4.63		(27)
Windows Type 5			4.53	x 1/[1/(1.4)+ 0.04]	= 6.01		(27)
Windows Type 6			6.9	x 1/[1/(1.4)+ 0.04]	= 9.15		(27)
Windows Type 7			1.73	x 1/[1/(1.4)+ 0.04]	= 2.29		(27)
Windows Type 8			2.25	x 1/[1/(1.4)+ 0.04]	= 2.98		(27)
Windows Type 9			2.25	x 1/[1/(1.4)+ 0.04]	= 2.98		(27)
Windows Type 10			2.25	x 1/[1/(1.4)+ 0.04]	= 2.98		(27)
Windows Type 11			1.05	x 1/[1/(1.4)+ 0.04]	= 1.39		(27)
Windows Type 12			1.05	x 1/[1/(1.4)+ 0.04]	= 1.39		(27)
Windows Type 13			1.05	x 1/[1/(1.4)+ 0.04]	= 1.39		(27)
Floor Type 1			65.15	x 0.17	= 11.0755		(28)
Floor Type 2			1.44	x 0.22	= 0.3168		(28)
Walls	170.96	33.78	137.18	x 0.19	= 26.06		(29)

DER WorkSheet: New dwelling design stage

Roof 66.59 0 66.59 × 0.11 = 7.32 (30)

Total area of elements, m² 304.14 (31)

* for windows and roof windows, use effective window U-value calculated using formula $1/[(1/U\text{-value})+0.04]$ as given in paragraph 3.2

** include the areas on both sides of internal walls and partitions

Fabric heat loss, W/K = S (A × U) (26)...(30) + (32) = 90.66 (33)

Heat capacity Cm = S(A × k) ((28)...(30) + (32) + (32a)...(32e) = 13745.16 (34)

Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m²K Indicative Value: Medium 250 (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f can be used instead of a detailed calculation.

Thermal bridges : S (L × Y) calculated using Appendix K 10.89 (36)

if details of thermal bridging are not known (36) = 0.05 × (31)

Total fabric heat loss (33) + (36) = 101.54 (37)

Ventilation heat loss calculated monthly (38)m = 0.33 × (25)m × (5)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(38)m=	58.71	58.37	58.05	56.51	56.23	54.89	54.89	54.64	55.41	56.23	56.81	57.41	(38)

Heat transfer coefficient, W/K (39)m = (37) + (38)m

(39)m=	160.25	159.92	159.59	158.06	157.77	156.43	156.43	156.19	156.95	157.77	158.35	158.96	
	Average = Sum(39) _{1...12} /12=											158.05	(39)

Heat loss parameter (HLP), W/m²K (40)m = (39)m ÷ (4)

(40)m=	1.39	1.39	1.39	1.38	1.37	1.36	1.36	1.36	1.37	1.37	1.38	1.38	
	Average = Sum(40) _{1...12} /12=											1.38	(40)

Number of days in month (Table 1a)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(41)m=	31	28	31	30	31	30	31	31	30	31	30	31	(41)

4. Water heating energy requirement: kWh/year:

Assumed occupancy, N 2.84 (42)

if TFA > 13.9, N = 1 + 1.76 × [1 - exp(-0.000349 × (TFA -13.9)²)] + 0.0013 × (TFA -13.9)

if TFA ≤ 13.9, N = 1

Annual average hot water usage in litres per day Vd,average = (25 × N) + 36 101.68 (43)

Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(44)m=	111.85	107.79	103.72	99.65	95.58	91.52	91.52	95.58	99.65	103.72	107.79	111.85	
	Total = Sum(44) _{1...12} =											1220.21	(44)

Energy content of hot water used - calculated monthly = 4.190 × Vd,m × nm × DTm / 3600 kWh/month (see Tables 1b, 1c, 1d)

(45)m=	165.87	145.07	149.7	130.52	125.23	108.07	100.14	114.91	116.28	135.52	147.93	160.64	
	Total = Sum(45) _{1...12} =											1599.89	(45)

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

(46)m=	24.88	21.76	22.46	19.58	18.78	16.21	15.02	17.24	17.44	20.33	22.19	24.1	(46)
--------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	------	------

Water storage loss:

Storage volume (litres) including any solar or WWHRS storage within same vessel 0 (47)

If community heating and no tank in dwelling, enter 110 litres in (47)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in (47)

Water storage loss:

DER WorkSheet: New dwelling design stage

a) If manufacturer's declared loss factor is known (kWh/day): (48)

0

Temperature factor from Table 2b (49)

0

Energy lost from water storage, kWh/year (48) x (49) = (50)

0

b) If manufacturer's declared cylinder loss factor is not known:

Hot water storage loss factor from Table 2 (kWh/litre/day) (51)

0

If community heating see section 4.3

Volume factor from Table 2a (52)

0

Temperature factor from Table 2b (53)

0

Energy lost from water storage, kWh/year (47) x (51) x (52) x (53) = (54)

0

Enter (50) or (54) in (55) (55)

0

Water storage loss calculated for each month ((56)m = (55) x (41)m

(56)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

(56)

If cylinder contains dedicated solar storage, (57)m = (56)m x [(50) - (H11)] ÷ (50), else (57)m = (56)m where (H11) is from Appendix H

(57)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

(57)

Primary circuit loss (annual) from Table 3 (58)

0

Primary circuit loss calculated for each month (59)m = (58) ÷ 365 x (41)m

(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat)

(59)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

(59)

Combi loss calculated for each month (61)m = (60) ÷ 365 x (41)m

(61)m=

14.15	12.77	14.12	13.62	14.04	13.55	13.98	14.02	13.59	14.08	13.67	14.14
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

(61)

Total heat required for water heating calculated for each month (62)m = 0.85 x (45)m + (46)m + (57)m + (59)m + (61)m

(62)m=

180.03	157.85	163.82	144.14	139.28	121.62	114.12	128.93	129.87	149.6	161.6	174.78
--------	--------	--------	--------	--------	--------	--------	--------	--------	-------	-------	--------

(62)

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)

(add additional lines if FGHRs and/or WWHRs applies, see Appendix G)

(63)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

(63)

Output from water heater

(64)m=

180.03	157.85	163.82	144.14	139.28	121.62	114.12	128.93	129.87	149.6	161.6	174.78
--------	--------	--------	--------	--------	--------	--------	--------	--------	-------	-------	--------

Output from water heater (annual)_{1...12} (64)

1765.63

Heat gains from water heating, kWh/month $0.25 \times [0.85 \times (45)m + (61)m] + 0.8 \times [(46)m + (57)m + (59)m]$

(65)m=

58.69	51.43	53.31	46.8	45.15	39.32	36.79	41.71	42.06	48.58	52.6	56.95
-------	-------	-------	------	-------	-------	-------	-------	-------	-------	------	-------

(65)

include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts

(66)m=

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
142.07	142.07	142.07	142.07	142.07	142.07	142.07	142.07	142.07	142.07	142.07	142.07

(66)

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5

(67)m=

24.83	22.05	17.93	13.58	10.15	8.57	9.26	12.03	16.15	20.51	23.94	25.52
-------	-------	-------	-------	-------	------	------	-------	-------	-------	-------	-------

(67)

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5

(68)m=

278.47	281.36	274.08	258.58	239.01	220.62	208.33	205.44	212.72	228.22	247.79	266.18
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

(68)

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5

(69)m=

37.21	37.21	37.21	37.21	37.21	37.21	37.21	37.21	37.21	37.21	37.21	37.21
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

(69)

Pumps and fans gains (Table 5a)

(70)m=

3	3	3	3	3	3	3	3	3	3	3	3
---	---	---	---	---	---	---	---	---	---	---	---

(70)

DER WorkSheet: New dwelling design stage

Losses e.g. evaporation (negative values) (Table 5)

(71)m=

-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66
---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------

 (71)

Water heating gains (Table 5)

(72)m=

78.89	76.53	71.65	65	60.69	54.61	49.45	56.07	58.42	65.3	73.06	76.54
-------	-------	-------	----	-------	-------	-------	-------	-------	------	-------	-------

 (72)

Total internal gains = (66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m

(73)m=

450.81	448.57	432.28	405.78	378.46	352.42	335.66	342.16	355.91	382.65	413.41	436.87
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

 (73)

6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

Orientation:	Access Factor Table 6d		Area m ²		Flux Table 6a		g_ Table 6b		FF Table 6c		Gains (W)							
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>7.31</td></tr></table> (74)	7.31
0.77																		
2.25																		
10.63																		
0.63																		
0.7																		
7.31																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.43</td></tr></table>	0.43	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>1.4</td></tr></table> (74)	1.4
0.77																		
0.43																		
10.63																		
0.63																		
0.7																		
1.4																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>7.31</td></tr></table> (74)	7.31
0.77																		
2.25																		
10.63																		
0.63																		
0.7																		
7.31																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>7.31</td></tr></table> (74)	7.31
0.77																		
2.25																		
10.63																		
0.63																		
0.7																		
7.31																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>7.31</td></tr></table> (74)	7.31
0.77																		
2.25																		
10.63																		
0.63																		
0.7																		
7.31																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>7.31</td></tr></table> (74)	7.31
0.77																		
2.25																		
10.63																		
0.63																		
0.7																		
7.31																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>13.97</td></tr></table> (74)	13.97
0.77																		
2.25																		
20.32																		
0.63																		
0.7																		
13.97																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.43</td></tr></table>	0.43	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>2.67</td></tr></table> (74)	2.67
0.77																		
0.43																		
20.32																		
0.63																		
0.7																		
2.67																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>13.97</td></tr></table> (74)	13.97
0.77																		
2.25																		
20.32																		
0.63																		
0.7																		
13.97																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>13.97</td></tr></table> (74)	13.97
0.77																		
2.25																		
20.32																		
0.63																		
0.7																		
13.97																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>13.97</td></tr></table> (74)	13.97
0.77																		
2.25																		
20.32																		
0.63																		
0.7																		
13.97																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>13.97</td></tr></table> (74)	13.97
0.77																		
2.25																		
20.32																		
0.63																		
0.7																		
13.97																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>23.74</td></tr></table> (74)	23.74
0.77																		
2.25																		
34.53																		
0.63																		
0.7																		
23.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.43</td></tr></table>	0.43	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>4.54</td></tr></table> (74)	4.54
0.77																		
0.43																		
34.53																		
0.63																		
0.7																		
4.54																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>23.74</td></tr></table> (74)	23.74
0.77																		
2.25																		
34.53																		
0.63																		
0.7																		
23.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>23.74</td></tr></table> (74)	23.74
0.77																		
2.25																		
34.53																		
0.63																		
0.7																		
23.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>23.74</td></tr></table> (74)	23.74
0.77																		
2.25																		
34.53																		
0.63																		
0.7																		
23.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>23.74</td></tr></table> (74)	23.74
0.77																		
2.25																		
34.53																		
0.63																		
0.7																		
23.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>38.14</td></tr></table> (74)	38.14
0.77																		
2.25																		
55.46																		
0.63																		
0.7																		
38.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.43</td></tr></table>	0.43	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>7.29</td></tr></table> (74)	7.29
0.77																		
0.43																		
55.46																		
0.63																		
0.7																		
7.29																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>38.14</td></tr></table> (74)	38.14
0.77																		
2.25																		
55.46																		
0.63																		
0.7																		
38.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>38.14</td></tr></table> (74)	38.14
0.77																		
2.25																		
55.46																		
0.63																		
0.7																		
38.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>38.14</td></tr></table> (74)	38.14
0.77																		
2.25																		
55.46																		
0.63																		
0.7																		
38.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>38.14</td></tr></table> (74)	38.14
0.77																		
2.25																		
55.46																		
0.63																		
0.7																		
38.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>51.38</td></tr></table> (74)	51.38
0.77																		
2.25																		
74.72																		
0.63																		
0.7																		
51.38																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.43</td></tr></table>	0.43	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>9.82</td></tr></table> (74)	9.82
0.77																		
0.43																		
74.72																		
0.63																		
0.7																		
9.82																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>51.38</td></tr></table> (74)	51.38
0.77																		
2.25																		
74.72																		
0.63																		
0.7																		
51.38																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>51.38</td></tr></table> (74)	51.38
0.77																		
2.25																		
74.72																		
0.63																		
0.7																		
51.38																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>51.38</td></tr></table> (74)	51.38
0.77																		
2.25																		
74.72																		
0.63																		
0.7																		
51.38																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>2.25</td></tr></table>	2.25	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>51.38</td></tr></table> (74)	51.38
0.77																		
2.25																		
74.72																		
0.63																		
0.7																		
51.38																		

DER WorkSheet: New dwelling design stage

North	0.9x	0.77	x	2.25	x	79.99	x	0.63	x	0.7	=	55	(74)
North	0.9x	0.77	x	0.43	x	79.99	x	0.63	x	0.7	=	10.51	(74)
North	0.9x	0.77	x	2.25	x	79.99	x	0.63	x	0.7	=	55	(74)
North	0.9x	0.77	x	2.25	x	79.99	x	0.63	x	0.7	=	55	(74)
North	0.9x	0.77	x	2.25	x	79.99	x	0.63	x	0.7	=	55	(74)
North	0.9x	0.77	x	2.25	x	79.99	x	0.63	x	0.7	=	55	(74)
North	0.9x	0.77	x	2.25	x	74.68	x	0.63	x	0.7	=	51.35	(74)
North	0.9x	0.77	x	0.43	x	74.68	x	0.63	x	0.7	=	9.81	(74)
North	0.9x	0.77	x	2.25	x	74.68	x	0.63	x	0.7	=	51.35	(74)
North	0.9x	0.77	x	2.25	x	74.68	x	0.63	x	0.7	=	51.35	(74)
North	0.9x	0.77	x	2.25	x	74.68	x	0.63	x	0.7	=	51.35	(74)
North	0.9x	0.77	x	2.25	x	74.68	x	0.63	x	0.7	=	51.35	(74)
North	0.9x	0.77	x	2.25	x	59.25	x	0.63	x	0.7	=	40.74	(74)
North	0.9x	0.77	x	0.43	x	59.25	x	0.63	x	0.7	=	7.79	(74)
North	0.9x	0.77	x	2.25	x	59.25	x	0.63	x	0.7	=	40.74	(74)
North	0.9x	0.77	x	2.25	x	59.25	x	0.63	x	0.7	=	40.74	(74)
North	0.9x	0.77	x	2.25	x	59.25	x	0.63	x	0.7	=	40.74	(74)
North	0.9x	0.77	x	2.25	x	59.25	x	0.63	x	0.7	=	40.74	(74)
North	0.9x	0.77	x	2.25	x	41.52	x	0.63	x	0.7	=	28.55	(74)
North	0.9x	0.77	x	0.43	x	41.52	x	0.63	x	0.7	=	5.46	(74)
North	0.9x	0.77	x	2.25	x	41.52	x	0.63	x	0.7	=	28.55	(74)
North	0.9x	0.77	x	2.25	x	41.52	x	0.63	x	0.7	=	28.55	(74)
North	0.9x	0.77	x	2.25	x	41.52	x	0.63	x	0.7	=	28.55	(74)
North	0.9x	0.77	x	2.25	x	41.52	x	0.63	x	0.7	=	28.55	(74)
North	0.9x	0.77	x	2.25	x	24.19	x	0.63	x	0.7	=	16.63	(74)
North	0.9x	0.77	x	0.43	x	24.19	x	0.63	x	0.7	=	3.18	(74)
North	0.9x	0.77	x	2.25	x	24.19	x	0.63	x	0.7	=	16.63	(74)
North	0.9x	0.77	x	2.25	x	24.19	x	0.63	x	0.7	=	16.63	(74)
North	0.9x	0.77	x	2.25	x	24.19	x	0.63	x	0.7	=	16.63	(74)
North	0.9x	0.77	x	2.25	x	24.19	x	0.63	x	0.7	=	16.63	(74)
North	0.9x	0.77	x	2.25	x	13.12	x	0.63	x	0.7	=	9.02	(74)
North	0.9x	0.77	x	0.43	x	13.12	x	0.63	x	0.7	=	1.72	(74)
North	0.9x	0.77	x	2.25	x	13.12	x	0.63	x	0.7	=	9.02	(74)
North	0.9x	0.77	x	2.25	x	13.12	x	0.63	x	0.7	=	9.02	(74)
North	0.9x	0.77	x	2.25	x	13.12	x	0.63	x	0.7	=	9.02	(74)
North	0.9x	0.77	x	2.25	x	8.86	x	0.63	x	0.7	=	6.1	(74)
North	0.9x	0.77	x	0.43	x	8.86	x	0.63	x	0.7	=	1.16	(74)
North	0.9x	0.77	x	2.25	x	8.86	x	0.63	x	0.7	=	6.1	(74)
North	0.9x	0.77	x	2.25	x	8.86	x	0.63	x	0.7	=	6.1	(74)
North	0.9x	0.77	x	2.25	x	8.86	x	0.63	x	0.7	=	6.1	(74)

DER WorkSheet: New dwelling design stage

North	0.9x	0.77	x	2.25	x	8.86	x	0.63	x	0.7	=	6.1	(74)
East	0.9x	0.77	x	1.73	x	19.64	x	0.63	x	0.7	=	10.38	(76)
East	0.9x	0.77	x	1.73	x	38.42	x	0.63	x	0.7	=	20.31	(76)
East	0.9x	0.77	x	1.73	x	63.27	x	0.63	x	0.7	=	33.45	(76)
East	0.9x	0.77	x	1.73	x	92.28	x	0.63	x	0.7	=	48.79	(76)
East	0.9x	0.77	x	1.73	x	113.09	x	0.63	x	0.7	=	59.79	(76)
East	0.9x	0.77	x	1.73	x	115.77	x	0.63	x	0.7	=	61.21	(76)
East	0.9x	0.77	x	1.73	x	110.22	x	0.63	x	0.7	=	58.27	(76)
East	0.9x	0.77	x	1.73	x	94.68	x	0.63	x	0.7	=	50.06	(76)
East	0.9x	0.77	x	1.73	x	73.59	x	0.63	x	0.7	=	38.91	(76)
East	0.9x	0.77	x	1.73	x	45.59	x	0.63	x	0.7	=	24.1	(76)
East	0.9x	0.77	x	1.73	x	24.49	x	0.63	x	0.7	=	12.95	(76)
East	0.9x	0.77	x	1.73	x	16.15	x	0.63	x	0.7	=	8.54	(76)
South	0.9x	0.77	x	3.49	x	46.75	x	0.63	x	0.7	=	49.87	(78)
South	0.9x	0.77	x	6.9	x	46.75	x	0.63	x	0.7	=	98.59	(78)
South	0.9x	0.77	x	1.05	x	46.75	x	0.63	x	0.7	=	15	(78)
South	0.9x	0.77	x	1.05	x	46.75	x	0.63	x	0.7	=	15	(78)
South	0.9x	0.77	x	1.05	x	46.75	x	0.63	x	0.7	=	15	(78)
South	0.9x	0.77	x	3.49	x	76.57	x	0.63	x	0.7	=	81.67	(78)
South	0.9x	0.77	x	6.9	x	76.57	x	0.63	x	0.7	=	161.46	(78)
South	0.9x	0.77	x	1.05	x	76.57	x	0.63	x	0.7	=	24.57	(78)
South	0.9x	0.77	x	1.05	x	76.57	x	0.63	x	0.7	=	24.57	(78)
South	0.9x	0.77	x	1.05	x	76.57	x	0.63	x	0.7	=	24.57	(78)
South	0.9x	0.77	x	3.49	x	97.53	x	0.63	x	0.7	=	104.03	(78)
South	0.9x	0.77	x	6.9	x	97.53	x	0.63	x	0.7	=	205.67	(78)
South	0.9x	0.77	x	1.05	x	97.53	x	0.63	x	0.7	=	31.3	(78)
South	0.9x	0.77	x	1.05	x	97.53	x	0.63	x	0.7	=	31.3	(78)
South	0.9x	0.77	x	1.05	x	97.53	x	0.63	x	0.7	=	31.3	(78)
South	0.9x	0.77	x	3.49	x	110.23	x	0.63	x	0.7	=	117.57	(78)
South	0.9x	0.77	x	6.9	x	110.23	x	0.63	x	0.7	=	232.45	(78)
South	0.9x	0.77	x	1.05	x	110.23	x	0.63	x	0.7	=	35.37	(78)
South	0.9x	0.77	x	1.05	x	110.23	x	0.63	x	0.7	=	35.37	(78)
South	0.9x	0.77	x	1.05	x	110.23	x	0.63	x	0.7	=	35.37	(78)
South	0.9x	0.77	x	3.49	x	114.87	x	0.63	x	0.7	=	122.52	(78)
South	0.9x	0.77	x	6.9	x	114.87	x	0.63	x	0.7	=	242.23	(78)
South	0.9x	0.77	x	1.05	x	114.87	x	0.63	x	0.7	=	36.86	(78)
South	0.9x	0.77	x	1.05	x	114.87	x	0.63	x	0.7	=	36.86	(78)
South	0.9x	0.77	x	1.05	x	114.87	x	0.63	x	0.7	=	36.86	(78)
South	0.9x	0.77	x	3.49	x	110.55	x	0.63	x	0.7	=	117.91	(78)
South	0.9x	0.77	x	6.9	x	110.55	x	0.63	x	0.7	=	233.12	(78)
South	0.9x	0.77	x	1.05	x	110.55	x	0.63	x	0.7	=	35.47	(78)

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South	0.9x	0.77	x	1.05	x	110.55	x	0.63	x	0.7	=	35.47	(78)
South	0.9x	0.77	x	1.05	x	110.55	x	0.63	x	0.7	=	35.47	(78)
South	0.9x	0.77	x	3.49	x	108.01	x	0.63	x	0.7	=	115.2	(78)
South	0.9x	0.77	x	6.9	x	108.01	x	0.63	x	0.7	=	227.77	(78)
South	0.9x	0.77	x	1.05	x	108.01	x	0.63	x	0.7	=	34.66	(78)
South	0.9x	0.77	x	1.05	x	108.01	x	0.63	x	0.7	=	34.66	(78)
South	0.9x	0.77	x	1.05	x	108.01	x	0.63	x	0.7	=	34.66	(78)
South	0.9x	0.77	x	3.49	x	104.89	x	0.63	x	0.7	=	111.88	(78)
South	0.9x	0.77	x	6.9	x	104.89	x	0.63	x	0.7	=	221.19	(78)
South	0.9x	0.77	x	1.05	x	104.89	x	0.63	x	0.7	=	33.66	(78)
South	0.9x	0.77	x	1.05	x	104.89	x	0.63	x	0.7	=	33.66	(78)
South	0.9x	0.77	x	1.05	x	104.89	x	0.63	x	0.7	=	33.66	(78)
South	0.9x	0.77	x	3.49	x	101.89	x	0.63	x	0.7	=	108.67	(78)
South	0.9x	0.77	x	6.9	x	101.89	x	0.63	x	0.7	=	214.85	(78)
South	0.9x	0.77	x	1.05	x	101.89	x	0.63	x	0.7	=	32.69	(78)
South	0.9x	0.77	x	1.05	x	101.89	x	0.63	x	0.7	=	32.69	(78)
South	0.9x	0.77	x	1.05	x	101.89	x	0.63	x	0.7	=	32.69	(78)
South	0.9x	0.77	x	3.49	x	82.59	x	0.63	x	0.7	=	88.08	(78)
South	0.9x	0.77	x	6.9	x	82.59	x	0.63	x	0.7	=	174.15	(78)
South	0.9x	0.77	x	1.05	x	82.59	x	0.63	x	0.7	=	26.5	(78)
South	0.9x	0.77	x	1.05	x	82.59	x	0.63	x	0.7	=	26.5	(78)
South	0.9x	0.77	x	1.05	x	82.59	x	0.63	x	0.7	=	26.5	(78)
South	0.9x	0.77	x	3.49	x	55.42	x	0.63	x	0.7	=	59.11	(78)
South	0.9x	0.77	x	6.9	x	55.42	x	0.63	x	0.7	=	116.86	(78)
South	0.9x	0.77	x	1.05	x	55.42	x	0.63	x	0.7	=	17.78	(78)
South	0.9x	0.77	x	1.05	x	55.42	x	0.63	x	0.7	=	17.78	(78)
South	0.9x	0.77	x	1.05	x	55.42	x	0.63	x	0.7	=	17.78	(78)
South	0.9x	0.77	x	3.49	x	40.4	x	0.63	x	0.7	=	43.09	(78)
South	0.9x	0.77	x	6.9	x	40.4	x	0.63	x	0.7	=	85.19	(78)
South	0.9x	0.77	x	1.05	x	40.4	x	0.63	x	0.7	=	12.96	(78)
South	0.9x	0.77	x	1.05	x	40.4	x	0.63	x	0.7	=	12.96	(78)
South	0.9x	0.77	x	1.05	x	40.4	x	0.63	x	0.7	=	12.96	(78)
West	0.9x	0.77	x	4.53	x	19.64	x	0.63	x	0.7	=	27.19	(80)
West	0.9x	0.77	x	4.53	x	38.42	x	0.63	x	0.7	=	53.19	(80)
West	0.9x	0.77	x	4.53	x	63.27	x	0.63	x	0.7	=	87.6	(80)
West	0.9x	0.77	x	4.53	x	92.28	x	0.63	x	0.7	=	127.76	(80)
West	0.9x	0.77	x	4.53	x	113.09	x	0.63	x	0.7	=	156.57	(80)
West	0.9x	0.77	x	4.53	x	115.77	x	0.63	x	0.7	=	160.28	(80)
West	0.9x	0.77	x	4.53	x	110.22	x	0.63	x	0.7	=	152.59	(80)
West	0.9x	0.77	x	4.53	x	94.68	x	0.63	x	0.7	=	131.07	(80)
West	0.9x	0.77	x	4.53	x	73.59	x	0.63	x	0.7	=	101.88	(80)

DER WorkSheet: New dwelling design stage

West	0.9x	0.77	x	4.53	x	45.59	x	0.63	x	0.7	=	63.11	(80)
West	0.9x	0.77	x	4.53	x	24.49	x	0.63	x	0.7	=	33.9	(80)
West	0.9x	0.77	x	4.53	x	16.15	x	0.63	x	0.7	=	22.36	(80)

Solar gains in watts, calculated for each month

(83)m = Sum(74)m ... (82)m

(83)m=	268.99	462.88	647.9	830.68	958.4	964.44	924.38	826.66	710.58	515.3	322.99	229.71	(83)
--------	--------	--------	-------	--------	-------	--------	--------	--------	--------	-------	--------	--------	------

Total gains – internal and solar (84)m = (73)m + (83)m , watts

(84)m=	719.8	911.44	1080.18	1236.46	1336.87	1316.86	1260.04	1168.83	1066.5	897.95	736.4	666.57	(84)
--------	-------	--------	---------	---------	---------	---------	---------	---------	--------	--------	-------	--------	------

7. Mean internal temperature (heating season)

Temperature during heating periods in the living area from Table 9, Th1 (°C)

21 (85)

Utilisation factor for gains for living area, h1,m (see Table 9a)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(86)m=	1	0.99	0.98	0.94	0.85	0.69	0.53	0.58	0.82	0.97	0.99	1	(86)

Mean internal temperature in living area T1 (follow steps 3 to 7 in Table 9c)

(87)m=	19.47	19.69	20.02	20.41	20.74	20.93	20.98	20.97	20.84	20.39	19.85	19.43	(87)
--------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	------

Temperature during heating periods in rest of dwelling from Table 9, Th2 (°C)

(88)m=	19.77	19.77	19.77	19.78	19.78	19.79	19.79	19.8	19.79	19.78	19.78	19.78	(88)
--------	-------	-------	-------	-------	-------	-------	-------	------	-------	-------	-------	-------	------

Utilisation factor for gains for rest of dwelling, h2,m (see Table 9a)

(89)m=	1	0.99	0.97	0.92	0.79	0.59	0.39	0.45	0.74	0.95	0.99	1	(89)
--------	---	------	------	------	------	------	------	------	------	------	------	---	------

Mean internal temperature in the rest of dwelling T2 (follow steps 3 to 7 in Table 9c)

(90)m=	18.39	18.62	18.94	19.33	19.62	19.76	19.79	19.79	19.7	19.32	18.78	18.36	(90)
--------	-------	-------	-------	-------	-------	-------	-------	-------	------	-------	-------	-------	------

fLA = Living area ÷ (4) =

0.28 (91)

Mean internal temperature (for the whole dwelling) = fLA × T1 + (1 – fLA) × T2

(92)m=	18.69	18.92	19.24	19.63	19.93	20.09	20.12	20.12	20.02	19.62	19.08	18.66	(92)
--------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	------

Apply adjustment to the mean internal temperature from Table 4e, where appropriate

(93)m=	18.69	18.92	19.24	19.63	19.93	20.09	20.12	20.12	20.02	19.62	19.08	18.66	(93)
--------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	------

8. Space heating requirement

Set Ti to the mean internal temperature obtained at step 11 of Table 9b, so that Ti,m=(76)m and re-calculate the utilisation factor for gains using Table 9a

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
--	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

Utilisation factor for gains, hm:

(94)m=	1	0.99	0.97	0.92	0.8	0.61	0.43	0.49	0.75	0.95	0.99	1	(94)
--------	---	------	------	------	-----	------	------	------	------	------	------	---	------

Useful gains, hmGm , W = (94)m x (84)m

(95)m=	716.56	900.35	1046.38	1133.24	1072.07	808.17	543.07	567.36	804.8	849.61	729.08	664.39	(95)
--------	--------	--------	---------	---------	---------	--------	--------	--------	-------	--------	--------	--------	------

Monthly average external temperature from Table 8

(96)m=	4.3	4.9	6.5	8.9	11.7	14.6	16.6	16.4	14.1	10.6	7.1	4.2	(96)
--------	-----	-----	-----	-----	------	------	------	------	------	------	-----	-----	------

Heat loss rate for mean internal temperature, Lm , W = [(39)m x [(93)m – (96)m]

(97)m=	2306.42	2241.69	2033.15	1696.04	1298.77	858.67	551.32	581.11	929.56	1422.81	1896.81	2298.16	(97)
--------	---------	---------	---------	---------	---------	--------	--------	--------	--------	---------	---------	---------	------

Space heating requirement for each month, kWh/month = 0.024 x [(97)m – (95)m] x (41)m

(98)m=	1182.86	901.38	734.16	405.21	168.66	0	0	0	0	426.46	840.76	1215.52	
--------	---------	--------	--------	--------	--------	---	---	---	---	--------	--------	---------	--

Total per year (kWh/year) = Sum(98)1...5,9...12 =

5875.02 (98)

Space heating requirement in kWh/m²/year

51.11 (99)

DER WorkSheet: New dwelling design stage

9a. Energy requirements – Individual heating systems including micro-CHP

Space heating:

Fraction of space heat from secondary/supplementary system		0	(201)
Fraction of space heat from main system(s)	(202) = 1 – (201) =	1	(202)
Fraction of total heating from main system 1	(204) = (202) × [1 – (203)] =	1	(204)
Efficiency of main space heating system 1		90.5	(206)
Efficiency of secondary/supplementary heating system, %		0	(208)

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	kWh/year
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	----------

Space heating requirement (calculated above)

1182.86	901.38	734.16	405.21	168.66	0	0	0	0	426.46	840.76	1215.52
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(211)m = {[[(98)m x (204)] } x 100 ÷ (206) (211)

1307.02	996	811.22	447.75	186.37	0	0	0	0	471.23	929.02	1343.12
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Total (kWh/year) =Sum(211)_{1...5,10...12}= 6491.74 (211)

Space heating fuel (secondary), kWh/month

= {[[(98)m x (201)] } x 100 ÷ (208)

(215)m=	0	0	0	0	0	0	0	0	0	0	0	
Total (kWh/year) =Sum(215) _{1...5,10...12} =												0 (215)

Water heating

Output from water heater (calculated above)

180.03	157.85	163.82	144.14	139.28	121.62	114.12	128.93	129.87	149.6	161.6	174.78
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Efficiency of water heater 87.3 (216)

(217)m=	90.06	90.01	89.9	89.64	89.02	87.3	87.3	87.3	87.3	89.65	89.97	90.08	(217)
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Fuel for water heating, kWh/month

(219)m = (64)m x 100 ÷ (217)m

(219)m=	199.89	175.37	182.23	160.8	156.45	139.31	130.72	147.69	148.77	166.88	179.61	194.02		
Total = Sum(219a) _{1...12} =													1981.74	(219)

Annual totals

	kWh/year	kWh/year
Space heating fuel used, main system 1		6491.74
Water heating fuel used		1981.74

Electricity for pumps, fans and electric keep-hot

central heating pump: 30 (230c)

boiler with a fan-assisted flue 45 (230e)

Total electricity for the above, kWh/year sum of (230a)...(230g) = 75 (231)

Electricity for lighting 438.43 (232)

12a. CO2 emissions – Individual heating systems including micro-CHP

	Energy kWh/year	Emission factor kg CO2/kWh		Emissions kg CO2/year
Space heating (main system 1)	(211) x	0.216	=	1402.22 (261)
Space heating (secondary)	(215) x	0.519	=	0 (263)
Water heating	(219) x	0.216	=	428.05 (264)
Space and water heating	(261) + (262) + (263) + (264) =			1830.27 (265)

DER WorkSheet: New dwelling design stage

Electricity for pumps, fans and electric keep-hot	(231) x	0.519	=	38.93	(267)
Electricity for lighting	(232) x	0.519	=	227.55	(268)
Total CO2, kg/year		sum of (265)...(271) =		2096.74	(272)
Dwelling CO2 Emission Rate		(272) ÷ (4) =		18.24	(273)
EI rating (section 14)				82	(274)

TER WorkSheet: New dwelling design stage

User Details:

Assessor Name: Demi Beneke **Stroma Number:** STRO027754
Software Name: Stroma FSAP 2012 **Software Version:** Version: 1.0.4.26

Property Address: Land Adj 11 Queen Annes Drive

Address : Land Adj 11 Queen Annes Drive

1. Overall dwelling dimensions:

	Area(m ²)		Av. Height(m)		Volume(m ³)
Ground floor	65.15 (1a)	x	2.6 (2a)	=	169.39 (3a)
First floor	49.79 (1b)	x	2.7 (2b)	=	134.43 (3b)
Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n)	114.94 (4)				
Dwelling volume				(3a)+(3b)+(3c)+(3d)+(3e)+.....(3n) =	303.82 (5)

2. Ventilation rate:

	main heating	secondary heating	other	total	m ³ per hour
Number of chimneys	0	0	0	0	0 (6a)
Number of open flues	0	0	0	0	0 (6b)
Number of intermittent fans				4	40 (7a)
Number of passive vents				0	0 (7b)
Number of flueless gas fires				0	0 (7c)

Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) =	40	÷ (5) =	0.13 (8)
<i>If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)</i>			
Number of storeys in the dwelling (ns)			0 (9)
Additional infiltration		[(9)-1]x0.1 =	0 (10)
Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction			0 (11)
<i>if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35</i>			
If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0			0 (12)
If no draught lobby, enter 0.05, else enter 0			0 (13)
Percentage of windows and doors draught stripped			0 (14)
Window infiltration	0.25 - [0.2 x (14) ÷ 100] =		0 (15)
Infiltration rate	(8) + (10) + (11) + (12) + (13) + (15) =		0 (16)
Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area			5 (17)
If based on air permeability value, then (18) = [(17) ÷ 20] + (8), otherwise (18) = (16)			0.38 (18)
<i>Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used</i>			
Number of sides sheltered			2 (19)
Shelter factor	(20) = 1 - [0.075 x (19)] =		0.85 (20)
Infiltration rate incorporating shelter factor	(21) = (18) x (20) =		0.32 (21)

Infiltration rate modified for monthly wind speed

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
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Monthly average wind speed from Table 7

(22)m=	5.1	5	4.9	4.4	4.3	3.8	3.8	3.7	4	4.3	4.5	4.7
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TER WorkSheet: New dwelling design stage

Wind Factor (22a)m = (22)m ÷ 4

(22a)m=	1.27	1.25	1.23	1.1	1.08	0.95	0.95	0.92	1	1.08	1.12	1.18
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Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

	0.41	0.41	0.4	0.36	0.35	0.31	0.31	0.3	0.32	0.35	0.36	0.38
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Calculate effective air change rate for the applicable case

If mechanical ventilation:

0 (23a)

If exhaust air heat pump using Appendix N, (23b) = (23a) × Fmv (equation (N5)) , otherwise (23b) = (23a)

0 (23b)

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

0 (23c)

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) × [1 – (23c) ÷ 100]

(24a)m=	0	0	0	0	0	0	0	0	0	0	0	0	(24a)
---------	---	---	---	---	---	---	---	---	---	---	---	---	-------

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

(24b)m=	0	0	0	0	0	0	0	0	0	0	0	0	(24b)
---------	---	---	---	---	---	---	---	---	---	---	---	---	-------

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 × (23b), then (24c) = (23b); otherwise (24c) = (22b) m + 0.5 × (23b)

(24c)m=	0	0	0	0	0	0	0	0	0	0	0	0	(24c)
---------	---	---	---	---	---	---	---	---	---	---	---	---	-------

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² x 0.5]

(24d)m=	0.59	0.58	0.58	0.56	0.56	0.55	0.55	0.55	0.55	0.56	0.57	0.57	(24d)
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Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

(25)m=	0.59	0.58	0.58	0.56	0.56	0.55	0.55	0.55	0.55	0.56	0.57	0.57	(25)
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3. Heat losses and heat loss parameter:

ELEMENT	Gross area (m²)	Openings m²	Net Area A ,m²	U-value W/m²K	A X U (W/K)	k-value kJ/m²·K	A X k kJ/K
Doors			2.3	x 1	= 2.3		(26)
Windows Type 1			1.89	x1/[1/(1.4)+ 0.04] =	2.51		(27)
Windows Type 2			0.36	x1/[1/(1.4)+ 0.04] =	0.48		(27)
Windows Type 3			1.89	x1/[1/(1.4)+ 0.04] =	2.51		(27)
Windows Type 4			2.93	x1/[1/(1.4)+ 0.04] =	3.88		(27)
Windows Type 5			3.8	x1/[1/(1.4)+ 0.04] =	5.04		(27)
Windows Type 6			5.79	x1/[1/(1.4)+ 0.04] =	7.68		(27)
Windows Type 7			1.45	x1/[1/(1.4)+ 0.04] =	1.92		(27)
Windows Type 8			1.89	x1/[1/(1.4)+ 0.04] =	2.51		(27)
Windows Type 9			1.89	x1/[1/(1.4)+ 0.04] =	2.51		(27)
Windows Type 10			1.89	x1/[1/(1.4)+ 0.04] =	2.51		(27)
Windows Type 11			0.88	x1/[1/(1.4)+ 0.04] =	1.17		(27)
Windows Type 12			0.88	x1/[1/(1.4)+ 0.04] =	1.17		(27)
Windows Type 13			0.88	x1/[1/(1.4)+ 0.04] =	1.17		(27)
Floor Type 1			65.15	x 0.13	= 8.4695		(28)
Floor Type 2			1.44	x 0.13	= 0.1872		(28)
Walls	170.96	28.72	142.24	x 0.18	= 25.6		(29)

TER WorkSheet: New dwelling design stage

Roof

 x

 =

 (30)

Total area of elements, m²

 (31)

* for windows and roof windows, use effective window U-value calculated using formula $1/[(1/U\text{-value})+0.04]$ as given in paragraph 3.2

** include the areas on both sides of internal walls and partitions

Fabric heat loss, W/K = S (A x U) (26)...(30) + (32) =

 (33)

Heat capacity Cm = S(A x k) ((28)...(30) + (32) + (32a)...(32e) =

 (34)

Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m²K Indicative Value: Medium

 (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f can be used instead of a detailed calculation.

Thermal bridges : S (L x Y) calculated using Appendix K

 (36)

if details of thermal bridging are not known (36) = 0.05 x (31)

Total fabric heat loss (33) + (36) =

 (37)

Ventilation heat loss calculated monthly (38)m = 0.33 x (25)m x (5)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(38)m=	58.71	58.37	58.05	56.51	56.23	54.89	54.89	54.64	55.41	56.23	56.81	57.41	(38)

Heat transfer coefficient, W/K (39)m = (37) + (38)m

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(39)m=	154.91	154.58	154.25	152.72	152.43	151.1	151.1	150.85	151.61	152.43	153.01	153.62	
Average = Sum(39) _{1...12} /12=												<table border="1" style="display: inline-table; width: 80px; text-align: center;">152.72</table>	(39)

Heat loss parameter (HLP), W/m²K (40)m = (39)m ÷ (4)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(40)m=	1.35	1.34	1.34	1.33	1.33	1.31	1.31	1.31	1.32	1.33	1.33	1.34	
Average = Sum(40) _{1...12} /12=												<table border="1" style="display: inline-table; width: 80px; text-align: center;">1.33</table>	(40)

Number of days in month (Table 1a)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(41)m=	31	28	31	30	31	30	31	31	30	31	30	31	(41)

4. Water heating energy requirement: kWh/year:

Assumed occupancy, N

 (42)

if TFA > 13.9, N = 1 + 1.76 x [1 - exp(-0.000349 x (TFA -13.9)²)] + 0.0013 x (TFA -13.9)

if TFA ≤ 13.9, N = 1

Annual average hot water usage in litres per day Vd,average = (25 x N) + 36

 (43)

Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(44)m=	111.85	107.79	103.72	99.65	95.58	91.52	91.52	95.58	99.65	103.72	107.79	111.85	
Total = Sum(44) _{1...12} =												<table border="1" style="display: inline-table; width: 80px; text-align: center;">1220.21</table>	(44)

Energy content of hot water used - calculated monthly = 4.190 x Vd,m x nm x DTm / 3600 kWh/month (see Tables 1b, 1c, 1d)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(45)m=	165.87	145.07	149.7	130.52	125.23	108.07	100.14	114.91	116.28	135.52	147.93	160.64	
Total = Sum(45) _{1...12} =												<table border="1" style="display: inline-table; width: 80px; text-align: center;">1599.89</table>	(45)

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(46)m=	24.88	21.76	22.46	19.58	18.78	16.21	15.02	17.24	17.44	20.33	22.19	24.1	(46)

Water storage loss:

Storage volume (litres) including any solar or WWHRS storage within same vessel

 (47)

If community heating and no tank in dwelling, enter 110 litres in (47)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in (47)

Water storage loss:

TER WorkSheet: New dwelling design stage

a) If manufacturer's declared loss factor is known (kWh/day): (48)

Temperature factor from Table 2b (49)

Energy lost from water storage, kWh/year (48) x (49) = (50)

b) If manufacturer's declared cylinder loss factor is not known:

Hot water storage loss factor from Table 2 (kWh/litre/day) (51)

If community heating see section 4.3

Volume factor from Table 2a (52)

Temperature factor from Table 2b (53)

Energy lost from water storage, kWh/year (47) x (51) x (52) x (53) = (54)

Enter (50) or (54) in (55) (55)

Water storage loss calculated for each month ((56)m = (55) x (41)m

(56)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

(56)

If cylinder contains dedicated solar storage, (57)m = (56)m x [(50) - (H11)] ÷ (50), else (57)m = (56)m where (H11) is from Appendix H

(57)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

(57)

Primary circuit loss (annual) from Table 3 (58)

Primary circuit loss calculated for each month (59)m = (58) ÷ 365 x (41)m

(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat)

(59)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

(59)

Combi loss calculated for each month (61)m = (60) ÷ 365 x (41)m

(61)m=

50.96	46.03	50.96	49.14	48.71	45.13	46.64	48.71	49.14	50.96	49.32	50.96
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

(61)

Total heat required for water heating calculated for each month (62)m = 0.85 x (45)m + (46)m + (57)m + (59)m + (61)m

(62)m=

216.83	191.1	200.66	179.66	173.94	153.2	146.78	163.62	165.43	186.48	197.24	211.6
--------	-------	--------	--------	--------	-------	--------	--------	--------	--------	--------	-------

(62)

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)

(add additional lines if FGHRs and/or WWHRs applies, see Appendix G)

(63)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

(63)

Output from water heater

(64)m=

216.83	191.1	200.66	179.66	173.94	153.2	146.78	163.62	165.43	186.48	197.24	211.6
--------	-------	--------	--------	--------	-------	--------	--------	--------	--------	--------	-------

(64)

Output from water heater (annual)_{1...12}

2186.54

Heat gains from water heating, kWh/month 0.25 ´ [0.85 x (45)m + (61)m] + 0.8 x [(46)m + (57)m + (59)m]

(65)m=

67.89	59.74	62.52	55.68	53.82	47.21	44.96	50.39	50.95	57.8	61.51	66.15
-------	-------	-------	-------	-------	-------	-------	-------	-------	------	-------	-------

(65)

include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts

(66)m=

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
142.07	142.07	142.07	142.07	142.07	142.07	142.07	142.07	142.07	142.07	142.07	142.07

(66)

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5

(67)m=

24.83	22.05	17.93	13.58	10.15	8.57	9.26	12.03	16.15	20.51	23.94	25.52
-------	-------	-------	-------	-------	------	------	-------	-------	-------	-------	-------

(67)

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5

(68)m=

278.47	281.36	274.08	258.58	239.01	220.62	208.33	205.44	212.72	228.22	247.79	266.18
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

(68)

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5

(69)m=

37.21	37.21	37.21	37.21	37.21	37.21	37.21	37.21	37.21	37.21	37.21	37.21
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

(69)

Pumps and fans gains (Table 5a)

(70)m=

3	3	3	3	3	3	3	3	3	3	3	3
---	---	---	---	---	---	---	---	---	---	---	---

(70)

TER WorkSheet: New dwelling design stage

Losses e.g. evaporation (negative values) (Table 5)

(71)m=

-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66	-113.66
---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------

 (71)

Water heating gains (Table 5)

(72)m=

91.25	88.91	84.03	77.34	72.33	65.58	60.42	67.72	70.76	77.69	85.44	88.91
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

 (72)

Total internal gains = (66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m

(73)m=

463.17	460.94	444.66	418.11	390.11	363.38	346.63	353.82	368.26	395.04	425.79	449.24
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

 (73)

6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

Orientation:	Access Factor Table 6d		Area m ²		Flux Table 6a		g_ Table 6b		FF Table 6c	=	Gains (W)							
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>6.14</td></tr></table> (74)	6.14
0.77																		
1.89																		
10.63																		
0.63																		
0.7																		
6.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.36</td></tr></table>	0.36	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>1.17</td></tr></table> (74)	1.17
0.77																		
0.36																		
10.63																		
0.63																		
0.7																		
1.17																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>6.14</td></tr></table> (74)	6.14
0.77																		
1.89																		
10.63																		
0.63																		
0.7																		
6.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>6.14</td></tr></table> (74)	6.14
0.77																		
1.89																		
10.63																		
0.63																		
0.7																		
6.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>6.14</td></tr></table> (74)	6.14
0.77																		
1.89																		
10.63																		
0.63																		
0.7																		
6.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>10.63</td></tr></table>	10.63	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>6.14</td></tr></table> (74)	6.14
0.77																		
1.89																		
10.63																		
0.63																		
0.7																		
6.14																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>11.74</td></tr></table> (74)	11.74
0.77																		
1.89																		
20.32																		
0.63																		
0.7																		
11.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.36</td></tr></table>	0.36	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>2.24</td></tr></table> (74)	2.24
0.77																		
0.36																		
20.32																		
0.63																		
0.7																		
2.24																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>11.74</td></tr></table> (74)	11.74
0.77																		
1.89																		
20.32																		
0.63																		
0.7																		
11.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>11.74</td></tr></table> (74)	11.74
0.77																		
1.89																		
20.32																		
0.63																		
0.7																		
11.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>11.74</td></tr></table> (74)	11.74
0.77																		
1.89																		
20.32																		
0.63																		
0.7																		
11.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>20.32</td></tr></table>	20.32	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>11.74</td></tr></table> (74)	11.74
0.77																		
1.89																		
20.32																		
0.63																		
0.7																		
11.74																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>19.94</td></tr></table> (74)	19.94
0.77																		
1.89																		
34.53																		
0.63																		
0.7																		
19.94																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.36</td></tr></table>	0.36	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>3.8</td></tr></table> (74)	3.8
0.77																		
0.36																		
34.53																		
0.63																		
0.7																		
3.8																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>19.94</td></tr></table> (74)	19.94
0.77																		
1.89																		
34.53																		
0.63																		
0.7																		
19.94																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>19.94</td></tr></table> (74)	19.94
0.77																		
1.89																		
34.53																		
0.63																		
0.7																		
19.94																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>19.94</td></tr></table> (74)	19.94
0.77																		
1.89																		
34.53																		
0.63																		
0.7																		
19.94																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>34.53</td></tr></table>	34.53	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>19.94</td></tr></table> (74)	19.94
0.77																		
1.89																		
34.53																		
0.63																		
0.7																		
19.94																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>32.04</td></tr></table> (74)	32.04
0.77																		
1.89																		
55.46																		
0.63																		
0.7																		
32.04																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.36</td></tr></table>	0.36	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>6.1</td></tr></table> (74)	6.1
0.77																		
0.36																		
55.46																		
0.63																		
0.7																		
6.1																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>32.04</td></tr></table> (74)	32.04
0.77																		
1.89																		
55.46																		
0.63																		
0.7																		
32.04																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>32.04</td></tr></table> (74)	32.04
0.77																		
1.89																		
55.46																		
0.63																		
0.7																		
32.04																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>32.04</td></tr></table> (74)	32.04
0.77																		
1.89																		
55.46																		
0.63																		
0.7																		
32.04																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>55.46</td></tr></table>	55.46	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>32.04</td></tr></table> (74)	32.04
0.77																		
1.89																		
55.46																		
0.63																		
0.7																		
32.04																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>43.16</td></tr></table> (74)	43.16
0.77																		
1.89																		
74.72																		
0.63																		
0.7																		
43.16																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>0.36</td></tr></table>	0.36	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>8.22</td></tr></table> (74)	8.22
0.77																		
0.36																		
74.72																		
0.63																		
0.7																		
8.22																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>43.16</td></tr></table> (74)	43.16
0.77																		
1.89																		
74.72																		
0.63																		
0.7																		
43.16																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>43.16</td></tr></table> (74)	43.16
0.77																		
1.89																		
74.72																		
0.63																		
0.7																		
43.16																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>43.16</td></tr></table> (74)	43.16
0.77																		
1.89																		
74.72																		
0.63																		
0.7																		
43.16																		
North	0.9x	<table><tr><td>0.77</td></tr></table>	0.77	x	<table><tr><td>1.89</td></tr></table>	1.89	x	<table><tr><td>74.72</td></tr></table>	74.72	x	<table><tr><td>0.63</td></tr></table>	0.63	x	<table><tr><td>0.7</td></tr></table>	0.7	=	<table><tr><td>43.16</td></tr></table> (74)	43.16
0.77																		
1.89																		
74.72																		
0.63																		
0.7																		
43.16																		

TER WorkSheet: New dwelling design stage

North	0.9x	0.77	x	1.89	x	79.99	x	0.63	x	0.7	=	46.2	(74)
North	0.9x	0.77	x	0.36	x	79.99	x	0.63	x	0.7	=	8.8	(74)
North	0.9x	0.77	x	1.89	x	79.99	x	0.63	x	0.7	=	46.2	(74)
North	0.9x	0.77	x	1.89	x	79.99	x	0.63	x	0.7	=	46.2	(74)
North	0.9x	0.77	x	1.89	x	79.99	x	0.63	x	0.7	=	46.2	(74)
North	0.9x	0.77	x	1.89	x	79.99	x	0.63	x	0.7	=	46.2	(74)
North	0.9x	0.77	x	1.89	x	74.68	x	0.63	x	0.7	=	43.13	(74)
North	0.9x	0.77	x	0.36	x	74.68	x	0.63	x	0.7	=	8.22	(74)
North	0.9x	0.77	x	1.89	x	74.68	x	0.63	x	0.7	=	43.13	(74)
North	0.9x	0.77	x	1.89	x	74.68	x	0.63	x	0.7	=	43.13	(74)
North	0.9x	0.77	x	1.89	x	74.68	x	0.63	x	0.7	=	43.13	(74)
North	0.9x	0.77	x	1.89	x	74.68	x	0.63	x	0.7	=	43.13	(74)
North	0.9x	0.77	x	1.89	x	59.25	x	0.63	x	0.7	=	34.22	(74)
North	0.9x	0.77	x	0.36	x	59.25	x	0.63	x	0.7	=	6.52	(74)
North	0.9x	0.77	x	1.89	x	59.25	x	0.63	x	0.7	=	34.22	(74)
North	0.9x	0.77	x	1.89	x	59.25	x	0.63	x	0.7	=	34.22	(74)
North	0.9x	0.77	x	1.89	x	59.25	x	0.63	x	0.7	=	34.22	(74)
North	0.9x	0.77	x	1.89	x	59.25	x	0.63	x	0.7	=	34.22	(74)
North	0.9x	0.77	x	1.89	x	41.52	x	0.63	x	0.7	=	23.98	(74)
North	0.9x	0.77	x	0.36	x	41.52	x	0.63	x	0.7	=	4.57	(74)
North	0.9x	0.77	x	1.89	x	41.52	x	0.63	x	0.7	=	23.98	(74)
North	0.9x	0.77	x	1.89	x	41.52	x	0.63	x	0.7	=	23.98	(74)
North	0.9x	0.77	x	1.89	x	41.52	x	0.63	x	0.7	=	23.98	(74)
North	0.9x	0.77	x	1.89	x	41.52	x	0.63	x	0.7	=	23.98	(74)
North	0.9x	0.77	x	1.89	x	24.19	x	0.63	x	0.7	=	13.97	(74)
North	0.9x	0.77	x	0.36	x	24.19	x	0.63	x	0.7	=	2.66	(74)
North	0.9x	0.77	x	1.89	x	24.19	x	0.63	x	0.7	=	13.97	(74)
North	0.9x	0.77	x	1.89	x	24.19	x	0.63	x	0.7	=	13.97	(74)
North	0.9x	0.77	x	1.89	x	24.19	x	0.63	x	0.7	=	13.97	(74)
North	0.9x	0.77	x	1.89	x	24.19	x	0.63	x	0.7	=	13.97	(74)
North	0.9x	0.77	x	1.89	x	13.12	x	0.63	x	0.7	=	7.58	(74)
North	0.9x	0.77	x	0.36	x	13.12	x	0.63	x	0.7	=	1.44	(74)
North	0.9x	0.77	x	1.89	x	13.12	x	0.63	x	0.7	=	7.58	(74)
North	0.9x	0.77	x	1.89	x	13.12	x	0.63	x	0.7	=	7.58	(74)
North	0.9x	0.77	x	1.89	x	13.12	x	0.63	x	0.7	=	7.58	(74)
North	0.9x	0.77	x	1.89	x	13.12	x	0.63	x	0.7	=	7.58	(74)
North	0.9x	0.77	x	1.89	x	8.86	x	0.63	x	0.7	=	5.12	(74)
North	0.9x	0.77	x	0.36	x	8.86	x	0.63	x	0.7	=	0.98	(74)
North	0.9x	0.77	x	1.89	x	8.86	x	0.63	x	0.7	=	5.12	(74)
North	0.9x	0.77	x	1.89	x	8.86	x	0.63	x	0.7	=	5.12	(74)
North	0.9x	0.77	x	1.89	x	8.86	x	0.63	x	0.7	=	5.12	(74)

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North	0.9x	0.77	x	1.89	x	8.86	x	0.63	x	0.7	=	5.12	(74)
East	0.9x	0.77	x	1.45	x	19.64	x	0.63	x	0.7	=	8.7	(76)
East	0.9x	0.77	x	1.45	x	38.42	x	0.63	x	0.7	=	17.03	(76)
East	0.9x	0.77	x	1.45	x	63.27	x	0.63	x	0.7	=	28.04	(76)
East	0.9x	0.77	x	1.45	x	92.28	x	0.63	x	0.7	=	40.89	(76)
East	0.9x	0.77	x	1.45	x	113.09	x	0.63	x	0.7	=	50.12	(76)
East	0.9x	0.77	x	1.45	x	115.77	x	0.63	x	0.7	=	51.3	(76)
East	0.9x	0.77	x	1.45	x	110.22	x	0.63	x	0.7	=	48.84	(76)
East	0.9x	0.77	x	1.45	x	94.68	x	0.63	x	0.7	=	41.95	(76)
East	0.9x	0.77	x	1.45	x	73.59	x	0.63	x	0.7	=	32.61	(76)
East	0.9x	0.77	x	1.45	x	45.59	x	0.63	x	0.7	=	20.2	(76)
East	0.9x	0.77	x	1.45	x	24.49	x	0.63	x	0.7	=	10.85	(76)
East	0.9x	0.77	x	1.45	x	16.15	x	0.63	x	0.7	=	7.16	(76)
South	0.9x	0.77	x	2.93	x	46.75	x	0.63	x	0.7	=	41.86	(78)
South	0.9x	0.77	x	5.79	x	46.75	x	0.63	x	0.7	=	82.73	(78)
South	0.9x	0.77	x	0.88	x	46.75	x	0.63	x	0.7	=	12.57	(78)
South	0.9x	0.77	x	0.88	x	46.75	x	0.63	x	0.7	=	12.57	(78)
South	0.9x	0.77	x	0.88	x	46.75	x	0.63	x	0.7	=	12.57	(78)
South	0.9x	0.77	x	2.93	x	76.57	x	0.63	x	0.7	=	68.56	(78)
South	0.9x	0.77	x	5.79	x	76.57	x	0.63	x	0.7	=	135.49	(78)
South	0.9x	0.77	x	0.88	x	76.57	x	0.63	x	0.7	=	20.59	(78)
South	0.9x	0.77	x	0.88	x	76.57	x	0.63	x	0.7	=	20.59	(78)
South	0.9x	0.77	x	0.88	x	76.57	x	0.63	x	0.7	=	20.59	(78)
South	0.9x	0.77	x	2.93	x	97.53	x	0.63	x	0.7	=	87.34	(78)
South	0.9x	0.77	x	5.79	x	97.53	x	0.63	x	0.7	=	172.59	(78)
South	0.9x	0.77	x	0.88	x	97.53	x	0.63	x	0.7	=	26.23	(78)
South	0.9x	0.77	x	0.88	x	97.53	x	0.63	x	0.7	=	26.23	(78)
South	0.9x	0.77	x	0.88	x	97.53	x	0.63	x	0.7	=	26.23	(78)
South	0.9x	0.77	x	2.93	x	110.23	x	0.63	x	0.7	=	98.71	(78)
South	0.9x	0.77	x	5.79	x	110.23	x	0.63	x	0.7	=	195.06	(78)
South	0.9x	0.77	x	0.88	x	110.23	x	0.63	x	0.7	=	29.65	(78)
South	0.9x	0.77	x	0.88	x	110.23	x	0.63	x	0.7	=	29.65	(78)
South	0.9x	0.77	x	0.88	x	110.23	x	0.63	x	0.7	=	29.65	(78)
South	0.9x	0.77	x	2.93	x	114.87	x	0.63	x	0.7	=	102.86	(78)
South	0.9x	0.77	x	5.79	x	114.87	x	0.63	x	0.7	=	203.26	(78)
South	0.9x	0.77	x	0.88	x	114.87	x	0.63	x	0.7	=	30.89	(78)
South	0.9x	0.77	x	0.88	x	114.87	x	0.63	x	0.7	=	30.89	(78)
South	0.9x	0.77	x	0.88	x	114.87	x	0.63	x	0.7	=	30.89	(78)
South	0.9x	0.77	x	2.93	x	110.55	x	0.63	x	0.7	=	98.99	(78)
South	0.9x	0.77	x	5.79	x	110.55	x	0.63	x	0.7	=	195.61	(78)
South	0.9x	0.77	x	0.88	x	110.55	x	0.63	x	0.7	=	29.73	(78)

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South	0.9x	0.77	x	0.88	x	110.55	x	0.63	x	0.7	=	29.73	(78)
South	0.9x	0.77	x	0.88	x	110.55	x	0.63	x	0.7	=	29.73	(78)
South	0.9x	0.77	x	2.93	x	108.01	x	0.63	x	0.7	=	96.72	(78)
South	0.9x	0.77	x	5.79	x	108.01	x	0.63	x	0.7	=	191.13	(78)
South	0.9x	0.77	x	0.88	x	108.01	x	0.63	x	0.7	=	29.05	(78)
South	0.9x	0.77	x	0.88	x	108.01	x	0.63	x	0.7	=	29.05	(78)
South	0.9x	0.77	x	0.88	x	108.01	x	0.63	x	0.7	=	29.05	(78)
South	0.9x	0.77	x	2.93	x	104.89	x	0.63	x	0.7	=	93.93	(78)
South	0.9x	0.77	x	5.79	x	104.89	x	0.63	x	0.7	=	185.61	(78)
South	0.9x	0.77	x	0.88	x	104.89	x	0.63	x	0.7	=	28.21	(78)
South	0.9x	0.77	x	0.88	x	104.89	x	0.63	x	0.7	=	28.21	(78)
South	0.9x	0.77	x	0.88	x	104.89	x	0.63	x	0.7	=	28.21	(78)
South	0.9x	0.77	x	2.93	x	101.89	x	0.63	x	0.7	=	91.23	(78)
South	0.9x	0.77	x	5.79	x	101.89	x	0.63	x	0.7	=	180.29	(78)
South	0.9x	0.77	x	0.88	x	101.89	x	0.63	x	0.7	=	27.4	(78)
South	0.9x	0.77	x	0.88	x	101.89	x	0.63	x	0.7	=	27.4	(78)
South	0.9x	0.77	x	0.88	x	101.89	x	0.63	x	0.7	=	27.4	(78)
South	0.9x	0.77	x	2.93	x	82.59	x	0.63	x	0.7	=	73.95	(78)
South	0.9x	0.77	x	5.79	x	82.59	x	0.63	x	0.7	=	146.14	(78)
South	0.9x	0.77	x	0.88	x	82.59	x	0.63	x	0.7	=	22.21	(78)
South	0.9x	0.77	x	0.88	x	82.59	x	0.63	x	0.7	=	22.21	(78)
South	0.9x	0.77	x	0.88	x	82.59	x	0.63	x	0.7	=	22.21	(78)
South	0.9x	0.77	x	2.93	x	55.42	x	0.63	x	0.7	=	49.62	(78)
South	0.9x	0.77	x	5.79	x	55.42	x	0.63	x	0.7	=	98.06	(78)
South	0.9x	0.77	x	0.88	x	55.42	x	0.63	x	0.7	=	14.9	(78)
South	0.9x	0.77	x	0.88	x	55.42	x	0.63	x	0.7	=	14.9	(78)
South	0.9x	0.77	x	0.88	x	55.42	x	0.63	x	0.7	=	14.9	(78)
South	0.9x	0.77	x	2.93	x	40.4	x	0.63	x	0.7	=	36.17	(78)
South	0.9x	0.77	x	5.79	x	40.4	x	0.63	x	0.7	=	71.48	(78)
South	0.9x	0.77	x	0.88	x	40.4	x	0.63	x	0.7	=	10.86	(78)
South	0.9x	0.77	x	0.88	x	40.4	x	0.63	x	0.7	=	10.86	(78)
South	0.9x	0.77	x	0.88	x	40.4	x	0.63	x	0.7	=	10.86	(78)
West	0.9x	0.77	x	3.8	x	19.64	x	0.63	x	0.7	=	22.81	(80)
West	0.9x	0.77	x	3.8	x	38.42	x	0.63	x	0.7	=	44.62	(80)
West	0.9x	0.77	x	3.8	x	63.27	x	0.63	x	0.7	=	73.48	(80)
West	0.9x	0.77	x	3.8	x	92.28	x	0.63	x	0.7	=	107.17	(80)
West	0.9x	0.77	x	3.8	x	113.09	x	0.63	x	0.7	=	131.34	(80)
West	0.9x	0.77	x	3.8	x	115.77	x	0.63	x	0.7	=	134.45	(80)
West	0.9x	0.77	x	3.8	x	110.22	x	0.63	x	0.7	=	128	(80)
West	0.9x	0.77	x	3.8	x	94.68	x	0.63	x	0.7	=	109.95	(80)
West	0.9x	0.77	x	3.8	x	73.59	x	0.63	x	0.7	=	85.46	(80)

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West	0.9x	0.77	x	3.8	x	45.59	x	0.63	x	0.7	=	52.94	(80)
West	0.9x	0.77	x	3.8	x	24.49	x	0.63	x	0.7	=	28.44	(80)
West	0.9x	0.77	x	3.8	x	16.15	x	0.63	x	0.7	=	18.76	(80)

Solar gains in watts, calculated for each month

(83)m = Sum(74)m ... (82)m

(83)m=	225.7	388.39	543.66	697.05	804.26	809.35	775.72	693.7	596.26	432.39	271.01	192.74	(83)
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Total gains – internal and solar (84)m = (73)m + (83)m , watts

(84)m=	688.88	849.33	988.32	1115.17	1194.37	1172.73	1122.35	1047.51	964.52	827.43	696.8	641.98	(84)
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7. Mean internal temperature (heating season)

Temperature during heating periods in the living area from Table 9, Th1 (°C)

21 (85)

Utilisation factor for gains for living area, h1,m (see Table 9a)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(86)m=	1	0.99	0.99	0.96	0.88	0.73	0.57	0.62	0.85	0.97	1	1	(86)

Mean internal temperature in living area T1 (follow steps 3 to 7 in Table 9c)

(87)m=	19.5	19.7	20	20.38	20.71	20.91	20.98	20.97	20.82	20.38	19.87	19.47	(87)
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Temperature during heating periods in rest of dwelling from Table 9, Th2 (°C)

(88)m=	19.8	19.81	19.81	19.82	19.82	19.83	19.83	19.83	19.83	19.82	19.82	19.81	(88)
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Utilisation factor for gains for rest of dwelling, h2,m (see Table 9a)

(89)m=	1	0.99	0.98	0.94	0.83	0.63	0.43	0.48	0.77	0.96	0.99	1	(89)
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Mean internal temperature in the rest of dwelling T2 (follow steps 3 to 7 in Table 9c)

(90)m=	17.82	18.12	18.55	19.1	19.54	19.77	19.82	19.82	19.68	19.11	18.36	17.78	(90)
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fLA = Living area ÷ (4) =

0.28 (91)

Mean internal temperature (for the whole dwelling) = fLA × T1 + (1 – fLA) × T2

(92)m=	18.29	18.56	18.96	19.46	19.87	20.09	20.15	20.14	20	19.47	18.79	18.25	(92)
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Apply adjustment to the mean internal temperature from Table 4e, where appropriate

(93)m=	18.29	18.56	18.96	19.46	19.87	20.09	20.15	20.14	20	19.47	18.79	18.25	(93)
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8. Space heating requirement

Set Ti to the mean internal temperature obtained at step 11 of Table 9b, so that Ti,m=(76)m and re-calculate the utilisation factor for gains using Table 9a

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
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Utilisation factor for gains, hm:

(94)m=	1	0.99	0.97	0.93	0.83	0.66	0.47	0.52	0.79	0.95	0.99	1	(94)
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Useful gains, hmGm , W = (94)m x (84)m

(95)m=	685.96	840.39	962.75	1039.34	996.6	770.36	525.85	548	758.69	789.46	690.51	639.97	(95)
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Monthly average external temperature from Table 8

(96)m=	4.3	4.9	6.5	8.9	11.7	14.6	16.6	16.4	14.1	10.6	7.1	4.2	(96)
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Heat loss rate for mean internal temperature, Lm , W = [(39)m x [(93)m – (96)m]

(97)m=	2167.92	2111.94	1922.13	1612.62	1244.91	830.04	535.92	564.36	894.97	1351.85	1788.14	2158.74	(97)
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Space heating requirement for each month, kWh/month = 0.024 x [(97)m – (95)m] x (41)m

(98)m=	1102.58	854.48	713.77	412.76	184.75	0	0	0	0	418.42	790.29	1129.96	(98)
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Total per year (kWh/year) = Sum(98)_{1...5,9...12} =

5607.02 (98)

Space heating requirement in kWh/m²/year

48.78 (99)

TER WorkSheet: New dwelling design stage

9a. Energy requirements – Individual heating systems including micro-CHP)

Space heating:

Fraction of space heat from secondary/supplementary system		0	(201)
Fraction of space heat from main system(s)	(202) = 1 – (201) =	1	(202)
Fraction of total heating from main system 1	(204) = (202) × [1 – (203)] =	1	(204)
Efficiency of main space heating system 1		93.4	(206)
Efficiency of secondary/supplementary heating system, %		0	(208)

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	kWh/year
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Space heating requirement (calculated above)

1102.58	854.48	713.77	412.76	184.75	0	0	0	0	418.42	790.29	1129.96
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(211)m = {[[(98)m x (204)] } x 100 ÷ (206) (211)

1180.49	914.86	764.21	441.93	197.8	0	0	0	0	447.99	846.14	1209.81
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Total (kWh/year) =Sum(211)_{1...5,10...12}= 6003.23 (211)

Space heating fuel (secondary), kWh/month

= {[[(98)m x (201)] } x 100 ÷ (208)

(215)m=	0	0	0	0	0	0	0	0	0	0	0
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Total (kWh/year) =Sum(215)_{1...5,10...12}= 0 (215)

Water heating

Output from water heater (calculated above)

216.83	191.1	200.66	179.66	173.94	153.2	146.78	163.62	165.43	186.48	197.24	211.6
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Efficiency of water heater 80.3 (216)

(217)m= 88.57 88.37 87.97 87.08 85.2 80.3 80.3 80.3 80.3 87.03 88.18 88.64 (217)

Fuel for water heating, kWh/month

(219)m = (64)m x 100 ÷ (217)m

(219)m=	244.82	216.26	228.1	206.32	204.15	190.78	182.78	203.76	206.01	214.28	223.67	238.71
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Total = Sum(219a)_{1...12} = 2559.64 (219)

Annual totals

	kWh/year	kWh/year
Space heating fuel used, main system 1	6003.23	
Water heating fuel used	2559.64	

Electricity for pumps, fans and electric keep-hot

central heating pump: 30 (230c)

boiler with a fan-assisted flue 45 (230e)

Total electricity for the above, kWh/year sum of (230a)...(230g) = 75 (231)

Electricity for lighting 438.43 (232)

12a. CO2 emissions – Individual heating systems including micro-CHP

	Energy kWh/year	Emission factor kg CO2/kWh		Emissions kg CO2/year
Space heating (main system 1)	(211) x	0.216	=	1296.7 (261)
Space heating (secondary)	(215) x	0.519	=	0 (263)
Water heating	(219) x	0.216	=	552.88 (264)
Space and water heating	(261) + (262) + (263) + (264) =			1849.58 (265)

TER WorkSheet: New dwelling design stage

Electricity for pumps, fans and electric keep-hot	(231) x	0.519	=	38.93	(267)
Electricity for lighting	(232) x	0.519	=	227.55	(268)
Total CO2, kg/year		sum of (265)...(271) =		2116.05	(272)
TER	=			18.41	(273)

SAP 2012 Overheating Assessment

Calculated by Stroma FSAP 2012 program, produced and printed on 01 September 2020

Property Details: Land Adj 11 Queen Annes Drive

Dwelling type:	Detached House
Located in:	England
Region:	South England
Cross ventilation possible:	Yes
Number of storeys:	2
Front of dwelling faces:	North
Overshading:	Average or unknown
Overhangs:	None
Thermal mass parameter:	Indicative Value Medium
Night ventilation:	True
Blinds, curtains, shutters:	None
Ventilation rate during hot weather (ach):	4 (Windows open half the time)

Overheating Details:

Summer ventilation heat loss coefficient:	401.05	(P1)
Transmission heat loss coefficient:	101.5	
Summer heat loss coefficient:	502.59	(P2)

Overhangs:

Orientation:	Ratio:	Z_overhangs:
North (W1)	0	1
North (W2)	0	1
North (W3)	0	1
South (W4)	0	1
West (W5)	0	1
South (W6)	0	1
East (W7)	0	1
North (W8)	0	1
North (W9)	0	1
North (W10)	0	1
South (W11)	0	1
South (W12)	0	1
South (W13)	0	1

Solar shading:

Orientation:	Z blinds:	Solar access:	Overhangs:	Z summer:	
North (W1)	1	0.9	1	0.9	(P8)
North (W2)	1	0.9	1	0.9	(P8)
North (W3)	1	0.9	1	0.9	(P8)
South (W4)	1	0.9	1	0.9	(P8)
West (W5)	1	0.9	1	0.9	(P8)
South (W6)	1	0.9	1	0.9	(P8)
East (W7)	1	0.9	1	0.9	(P8)
North (W8)	1	0.9	1	0.9	(P8)
North (W9)	1	0.9	1	0.9	(P8)
North (W10)	1	0.9	1	0.9	(P8)
South (W11)	1	0.9	1	0.9	(P8)
South (W12)	1	0.9	1	0.9	(P8)
South (W13)	1	0.9	1	0.9	(P8)

Solar gains:

Orientation	Area	Flux	g_	FF	Shading	Gains
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SAP 2012 Overheating Assessment

North (W1)	0.9 x	2.25	87.17	0.63	0.7	0.9	70.06
North (W2)	0.9 x	0.43	87.17	0.63	0.7	0.9	13.39
North (W3)	0.9 x	2.25	87.17	0.63	0.7	0.9	70.06
South (W4)	0.9 x	3.49	118.56	0.63	0.7	0.9	147.8
West (W5)	0.9 x	4.53	125.28	0.63	0.7	0.9	202.73
South (W6)	0.9 x	6.9	118.56	0.63	0.7	0.9	292.21
East (W7)	0.9 x	1.73	125.28	0.63	0.7	0.9	77.42
North (W8)	0.9 x	2.25	87.17	0.63	0.7	0.9	70.06
North (W9)	0.9 x	2.25	87.17	0.63	0.7	0.9	70.06
North (W10)	0.9 x	2.25	87.17	0.63	0.7	0.9	70.06
South (W11)	0.9 x	1.05	118.56	0.63	0.7	0.9	44.47
South (W12)	0.9 x	1.05	118.56	0.63	0.7	0.9	44.47
South (W13)	0.9 x	1.05	118.56	0.63	0.7	0.9	44.47
Total							1217.25 (P3/P4)

Internal gains:

	June	July	August
Internal gains	517.03	495.25	504.49
Total summer gains	1819.68	1712.51	1610.54 (P5)
Summer gain/loss ratio	3.62	3.41	3.2 (P6)
Mean summer external temperature (South England)	15.4	17.3	17.3
Thermal mass temperature increment	0.25	0.25	0.25
Threshold temperature	19.27	20.96	20.75 (P7)
Likelihood of high internal temperature	Not significant	Slight	Slight

Assessment of likelihood of high internal temperature: Slight