



Land off Hermitage Park
Harts Farm Way, Havant, PO9 1HS

Noise Impact Assessment

12th January 2026
Revision 2



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Revision History

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Executive Summary and Conclusions

ParkerJones Acoustics Limited (PJA) has prepared this updated Noise Impact Assessment for the proposed gas-fuelled capacity mechanism embedded generation plant at Land off Hermitage Park, Harts Farm Way, Havant, PO9 1HS.

This report (Revision 2) updates PJA's previous assessment (Revision 1, submitted in support of planning application APP/24/00237) to reflect a revised site layout now proposed for the development. The updated layout has been compared against the earlier Royal HaskoningDHV UK Ltd assessment (July 2017, APP/21/00809) and PJA's 2024 assessment (Revision 1) to determine whether the new configuration would result in any material change in noise impact at nearby noise-sensitive receptors.

The assessment has been undertaken in accordance with BS 4142:2014 + A1:2019, using detailed noise modelling and the background sound levels established from the original baseline survey. The predicted noise levels from the revised layout are lower than both previous assessments, remaining at least 14 dB below typical daytime background levels and comfortably within the BS 8233:2014 internal noise criteria for dwellings, even with partially open windows.

The predicted specific noise levels from the proposed layout are 39 dB at NSR 1 and 43 dB at NSR 2, which are 5 dB and 3 dB lower respectively than the corresponding levels predicted in the 2017 Royal HaskoningDHV assessment, and equivalent or up to 1 dB lower than those predicted in PJA's 2024 (Revision 1) assessment. The results therefore confirm that the revised layout would not result in any material increase in noise impact relative to the previously approved schemes and can be considered acoustically equivalent or better.

At these levels, noise emissions during peak operation are considered unlikely to result in any adverse impact on the nearest residential receptors. The predicted levels would also satisfy the internal ambient noise targets of BS 8233:2014 within nearby dwellings, even with partially open windows.

The findings of the Construction Noise and Vibration Assessment previously issued by PJA (18 February 2022, APP/21/00809) also remain valid. The proposed amendments to the layout and plant arrangement would not materially alter the anticipated construction methods, and the earlier conclusions remain applicable—namely, that the identified noise and vibration limits are unlikely to be exceeded, provided that the Construction Noise Management Plan (as detailed in that report) is implemented and that Best Practicable Means continue to be applied to minimise emissions.

Accordingly, noise should not pose a constraint to the granting of planning permission for the proposed development.

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1.0 Introduction

ParkerJones Acoustics Limited (PJA) has been instructed to undertake an updated Noise Impact Assessment for the proposed *"Gas-fuelled Capacity Mechanism Embedded Generation Plant to support the National Grid"* at Land off Hermitage Park, Harts Farm Way, Havant, PO9 1HS.

This report constitutes Revision 2 of PJA's previous Noise Impact Assessment (Revision 1), which supported planning application APP/24/00237. The purpose of this update is to assess a revised site layout and to compare its predicted noise emissions against those from both previously approved schemes on the same site.

Specifically, this assessment compares the operational noise impact of the current layout with:

- the Royal HaskoningDHV UK Ltd assessment (July 2017), submitted in support of APP/21/00809; and
- the PJA Noise Impact Assessment (Revision 1), prepared in support of APP/24/00237, which introduced an updated site layout and generator technology following transfer of ownership of the site.

The present revision considers a new configuration of plant and equipment within the site and determines whether it would result in any material change in the predicted noise impact relative to the approved 2017 and 2024 layouts.

1.1 Scope of Report

The aims of this assessment are to:

- predict the operational noise emissions from the revised layout using the latest equipment information and 3-D CadnaA modelling;
- compare those emissions against the representative background noise levels previously established for the site;
- benchmark the results against the criteria and conclusions of the earlier 2017 and 2024 studies; and
- determine whether the revised layout maintains an equivalent or lower impact at the nearest residential receptors.

The background sound levels used in this assessment are based on the baseline noise survey undertaken by Royal HaskoningDHV UK Ltd (2017), which remain representative given the commercial nature of the surrounding area.

As before, the objective is to ensure that the risk of adverse impact from operational noise is sufficiently controlled such that the development will not cause a significant increase in external ambient noise levels at neighbouring properties once operational.

Whilst every attempt has been made to ensure that this report communicates effectively to a reader who might not have much knowledge of acoustics, some parts are necessarily technical. A glossary of acoustic terminology and concepts is provided in **Appendix A**.

1.2 Regulations and Guidelines

This report takes into consideration national planning policies including the National Planning Policy Framework (NPPF), the Noise Policy Statement for England (NPSE) and the Planning Practice Guidance on Noise (PPG-N) (summarised in **Appendix B**), which outline the purpose and long-term vision of planning policy with respect to noise. The assessment is aimed at limiting the impacts to no greater than the Lowest Observed Adverse Effect Level (the level above which adverse effects on health and quality of life can be detected).

More specifically, the assessment has been undertaken with reference to:

- BS 4142:2014+A1:2019 'Methods for rating and assessing industrial and commercial sound', which assesses the risk of an adverse impact of noise pollution from a sound source (or sources) of a commercial or industrial nature (i.e., mechanical/electrical plant);
- BS 8233:2014 'Guidance on Sound Insulation and Noise Reduction for Buildings'; and
- the WHO Environmental Noise Guidelines for the European Region.

2.0 Site and Development Description

The application site is located at Land off Hermitage Park, Harts Farm Way, Havant, PO9 1HS (northing 105818, easting 470601).

As shown in **Figure 2.1**, the site lies within an established commercial and industrial area, bounded by the A27 Havant Bypass to the north, Harts Farm Way to the south, and other commercial premises to the east and west. The land itself is currently unused.

The nearest residential receptors are located on Mill Lane, approximately 380 m to the north-west, and on Brockhampton Road, approximately 450 m to the north-east.

The site already benefits from planning consent for a gas-fuelled capacity mechanism generation plant (ref. APP/21/00809), which was subsequently revised under APP/24/00237 to reflect changes to the layout and generating technology.

The current proposals are of a similar nature, comprising eight containerised gas-engine generator units, each rated at approximately 2.5 MW electrical output. Each generator is housed within an acoustic container, with air intakes and air outlets positioned at either end of the unit, both fitted with in-duct silencers. An exhaust flue protrudes vertically from the roof of each container, also incorporating an in-duct silencer. Eight roof-mounted radiators are provided for engine cooling.

Associated electrical infrastructure includes one 33 kV transformer and one 11/0.415 kV transformer.

The general arrangement of the proposed equipment is illustrated in **Figure 2.2 (site layout)**.

The primary function of the development remains to provide flexible, short-term backup electricity supply to the local network during periods of peak demand or reduced grid capacity.

Figure 2.1 – Aerial view of the site and surrounding area



Figure 2.2 – Proposed site plan



3.0 Planning History and Relevant Guidelines

3.1 Previous Assessments

3.1.1 Royal HaskoningDHV (2017) Assessment

The first assessment of noise at the site was undertaken by Royal HaskoningDHV UK Ltd on behalf of Green Frog Power II Ltd, reported in “Proposed Peak Power Generation Facility – Harts Farm Way, Havant” (ref. I&BPB5588-111-100R001F02, July 2017).

That report supported planning application APP/21/00809 and considered a scheme comprising fourteen containerised gas-fired generator units arranged within a fenced compound. A baseline environmental noise survey was undertaken to establish representative background sound levels at two monitoring positions:

- MP1 (NSR 1) – to the north-east of the site, representing residential properties along Brockhampton Road, Ranelagh Road, Doyle Close, Abrams Way and Longcroft Way; and
- MP2 (NSR 2) – to the north-west, representing residential properties on Mill Lane.

Both positions were selected as being representative of the nearest residential receptors to the proposed development. Further detail on the baseline noise survey is provided in **Section 4.1.1** of this report.

Noise predictions were undertaken using SoundPLAN modelling software in accordance with ISO 9613-2 propagation methodology. All fourteen generators were assumed to operate simultaneously under worst-case conditions, with source sound power levels derived from manufacturer data for the engine containers, exhaust outlets and cooling systems.

The model predicted specific noise levels of:

- 44 dB L_{Aeq} at NSR 1; and
- 46 dB L_{Aeq} at NSR 2,

both rounded to 0 decimal places (**Table 5.1** of the 2017 report). When compared with the representative background levels, the assessment concluded that the proposed development would operate well below existing ambient noise conditions, corresponding to a “no adverse impact” outcome under BS 4142:2014.

3.1.2 ParkerJones Acoustics (2024) Assessment

A further Noise Impact Assessment was undertaken by ParkerJones Acoustics Limited (PJA) in February 2024 (issued as Revision 1 of this report) in support of planning application APP/24/00237. This related to an alternative layout for the site comprising five containerised gas-fuelled generator units, each rated at approximately 4.5 MW, together with associated exhaust stacks, cooling systems, and transformers.

The same nearest residential receptors were considered as in the 2017 assessment — namely NSR 1 (residential properties along Brockhampton Road, Ranelagh Road, Doyle Close, Abrams Way and Longcroft Way) and NSR 2 (properties on Mill Lane).

Noise predictions were undertaken using CadnaA modelling software in accordance with ISO 9613-2 propagation methodology. The model assumed all generator units operating simultaneously under worst-case conditions, with source sound power levels based on manufacturer data for the engine enclosures, air intakes, air outlets, exhaust stacks and radiators.

The predicted specific noise levels were:

- 39 dB L_{Aeq} at NSR 1; and
- 44 dB L_{Aeq} at NSR 2,

both rounded to 0 decimal places. These are lower than the levels predicted in the 2017 Royal HaskoningDHV report (44 dB and 46 dB respectively), reflecting the reduced number of generating units and improved acoustic performance of the plant enclosures.

The assessment concluded that the development would operate well below existing background noise levels, indicating a low likelihood of adverse impact in accordance with BS 4142:2014+A1:2019.

3.2 BS 4142:2014

BS 4142:2014 '*Methods for rating and assessing industrial and commercial sound*' is intended to be used to assess the potential adverse impact of sound of an industrial and/or commercial nature, at nearby noise-sensitive receptor (NSR) locations (i.e., residential windows) within the context of the existing sound environment.

The method is based upon assessing the predicted noise emissions from plant/equipment against the existing background sound levels at NSRs, the latter of which is determined by a noise survey conducted at the site.

The predicted noise emissions are termed as a 'rating level', which is the 'specific sound level' from plant (the actual measurable noise level), plus 'penalties' which account for whether the noise has distinguishing characteristics such as tonality, intermittency, impulsivity, or is generally distinguishable from the ambient noise environment. Such features may attract attention and be considered annoying, hence sounds with these qualities should be penalised over sounds at the same specific noise level which is less intrusive.

The general aim is for the 'rating level' (plant noise emissions) to not exceed the existing background sound levels outside of residential windows. BS 4142:2014 states that *"the lower the rating level is relative to the measured background sound level, the less likely it is that the specific sound source will have an adverse impact or a significant adverse impact. Where the rating level does not exceed the background sound level, this is an indication of the specific sound source having a low impact, depending on the context."*

Appendix B.4 explains the methodology in further detail.

3.3 BS 8233:2014

BS 8233:2014 'Guidance on Sound Insulation and Noise Reduction for Buildings' suggests appropriate criteria and limits for different situations.

Table 4 of BS 8233:2014 provides internal ambient noise level (IANL) limits for dwellings from "steady external noise sources". These are summarised in **Table 3.1** below.

Table 3.1 – BS 8233:2014 internal ambient noise level (IANL) upper limits

Activity	Location	Daytime (07:00 – 23:00)	Nighttime (23:00 – 07:00)
Resting	Living Room	35 dB $L_{Aeq,16hr}$	-
Dining	Dining Room/Area	40 dB $L_{Aeq,16hr}$	-
Sleeping (daytime resting)	Bedroom	35 dB $L_{Aeq,16hr}$	30 dB $L_{Aeq,8hr}$

Annex G.1 of BS 8233:2014 suggests that "if partially open windows were relied upon for background ventilation, the insulation would be reduced to approximately 15 dB". Therefore, a noise limit directly outside of the nearest residential windows could be set based on the values above plus 15 dB.

Therefore, to meet internal noise targets in nearby residential dwellings, noise from the proposed plant should not exceed 50 dB L_{Aeq} during the daytime and 45 dB L_{Aeq} during the nighttime when measured/calculated directly outside of a residential bedroom or living room window.

3.4 World Health Organisation (WHO) Environmental Noise Guidelines

The WHO document *Guidelines for Community Noise 1999* has recently been superseded by the *Environmental Noise Guidelines for the European Region*. However, the updated guidance states that 'all WHO guidelines for community noise (CNG) indoor guideline values and any values not covered by the current guidelines (such as industrial noise and shopping areas) should remain valid'.

The document sets out guidance as to noise levels at which there will be an unacceptable impact on the local community. WHO guidelines state:

- To protect the majority of people from being seriously annoyed during the daytime, the sound pressure level on balconies, terraces and outdoor living areas should not exceed 55 dB L_{Aeq} for a steady, continuous noise.
- To protect the majority of people from being moderately annoyed during the daytime, the outdoor sound pressure level should not exceed 50 dB L_{Aeq} .

4.0 Assessment

4.1 Operational Noise

The assessment has been undertaken in accordance with BS 4142:2014+A1:2019. The following summarises the main steps of action in the assessment method:

- a representative background sound level $L_{A90,Tr}$ is determined based upon the results of an environmental noise survey conducted as part of the previous planning application by *HaskoningDHV UK Ltd*.
- the specific sound level L_s generated by the proposed plant is predicted outside of the windows of neighbouring noise-sensitive windows in the area and residential gardens;
- the rating level $L_{A,r,Tr}$ is determined by the application of any 'penalties' which adjust for characteristic features of the sound which may be perceptible and potentially cause annoyance at each NSR;
- the predicted rating level $L_{A,r,Tr}$ is compared to the $L_{A90,Tr}$ and the recommendations of BS 4142:2014+A1:2019;
- the predicted specific noise levels are also compared against the guidelines of the WHO and BS 8233:2014, to provide further 'context' to the results (as referenced by BS 4142:2014+A1:2019);
- results are also benchmarked against the findings of the previous 2017 assessment by HaskoningDHV UK Ltd (summarised in **Section 3.1.1**) and the 2024 assessment by ParkerJones Acoustics (summarised in **Section 3.1.2**).

4.1.1 Background Sound Levels

In accordance with BS 4142:2014, the predicted rating level should be assessed against a 'representative' background sound level. This is commonly determined through the results of a baseline sound survey.

A baseline noise survey at two monitoring positions close to the nearby residential receptors (those highlighted in **Figure 2.1**) has previously been conducted by *HaskoningDHV UK Ltd* and submitted with the most recent successful planning application at the site – report reference I&BPB5588-111-100R001F02 dated July 2017 ¹.

The survey was conducted on the 4th and 5th of July 2017 during the daytime and nighttime. The survey results should still be valid/worst-case, given the amount of development in the area, it is highly unlikely that baseline levels would have decreased since these surveys were carried out. Given that the survey was conducted at the nearest residents assessed herein, using the same methodology that PJA would have used, the results are appropriate to use here. It appears that the survey:

- used Class 1 sound measuring equipment which was within calibration;
- was conducted by a consultant sufficiently qualified and competent in environmental noise monitoring;
- was conducted in appropriate weather conditions (dry with low wind speeds);
- was conducted at representative measurement positions;

1 - https://planningpublicaccess.havant.gov.uk/online-applications/files/81E1ED7C9AE583DA77A1503C48EEC3D1/pdf/APP_21_00809-APPENDIX E APPROVED NOISE ASSESSMENT-1515441.pdf

- generally followed the guidelines of British Standard 7445: 2003: Description and measurement of environmental noise;

The survey determined the following representative background sound levels (**Table 4.1**).

For the assessment, given the minimal chance of nighttime operation, only the daytime levels are relevant.

Table 4.1 – Derived representative background sound level $L_{A90, T}$ at nearby NSRs

Noise-Sensitive Receptor (NSR)	Period	Representative Background Sound Level L_{A90} (dB)
NSR 1 (Position P1)	Daytime (07:00 to 23:00)	57
	Nighttime (23:00 – 07:00)	42
NSR 2 (Position P2)	Daytime (07:00 to 23:00)	57
	Nighttime (23:00 – 07:00)	42

4.1.2 Proposed Plant

The input data used in the noise modelling is based on the description of noise sources outlined in **Section 2.0**. The data has been derived primarily from the report “Gas Generator Set – Noise Assessment” (ref. 15487-SRL-RP-YA-001-P1, dated 22nd July 2020) prepared by SRL Technical Services Ltd for Yellow Power Ltd.

That report was commissioned to verify the acoustic performance of the containerised generator design under controlled (“laboratory-type”) conditions, in order to validate manufacturer claims of approximately 72 dB(A) at 1 m under free-field conditions. SRL undertook detailed analysis of the generator assembly, including the engine enclosure, air-intake and outlet attenuators, radiator fans, and exhaust system, measuring octave-band sound power and sound pressure levels for each component and confirming overall emissions through 3D noise mapping. Their results indicated average free-field levels of approximately 72 dB(A) at 1 m, with localised peaks of up to 75 dB(A) at ground level around certain positions of the container.

For the current assessment, ParkerJones Acoustics Ltd (PJA) has replicated the SRL acoustic model as closely as practicable, using the same component sound power spectra, insertion losses, and sound reduction indices. This enables the acoustic behaviour demonstrated in SRL’s controlled testing to be translated into a site-specific CadnaA model for the Harts Farm Way development.

Each generator unit within the model has been represented using a combination of point sources, area sources, and a building object, as follows:

- The container itself has been modelled as a building element, using the plan dimensions shown on the layout drawings and an overall height of 3.55 m.
- Radiator fans have been modelled as individual point sources (8 per container), positioned above each generator container at a height of 4.65 m, with the sound power levels taken from **Table 4.2**.
- Air inlets and air outlets have been modelled as area sources located at either end of each container, representing the louvred ventilation openings, with corresponding sound power levels from **Table 4.2** and insertion losses for the attenuators applied (from **Table 4.3**).
- The exhaust outlets (flues) have been modelled as point sources located at 12.0 m above ground level (sound pressure levels for the unattenuated outlet in **Table 4.3**), incorporating the attenuation provided by the in-duct silencer (**Table 4.4**, which reduces the source level substantially). A secondary point source has been included to represent regenerated noise from the silencer (SPL given in **Table 4.3**).
- Container walls and roof panels have been modelled as vertical and horizontal area sources, derived from the internal sound pressure levels in **Table 4.3** and applying the sound reduction indices (SRI) of the container construction (**Table 4.4**).
- Transformers have been modelled as point sources at a height of 2.0 m, with sound power levels from **Table 4.2**, consistent with those adopted in the previous assessments (including Revision 1 of this report). These items are independent of the SRL testing and represent the auxiliary transformers forming part of the site's electrical infrastructure.

A total of eight generator units have been modelled in accordance with the latest site layout, with the combined contribution of all plant items considered under worst-case simultaneous operation.

Table 4.2 – Sound Power Levels of Air Inlet and Outlet Louvres, Radiator Fans and Transformers

Equipment	Quantity	Location	Sound Power Levels (SWL), dB								
			Octave Band Centre Frequencies, Hz (Unweighted values)								dB(A)
			63	125	250	500	1 k	2 k	4 k	8 k	
Air Intake	1 per container	Inside container / intaking from one end	85	89	88	86	82	83	80	77	90
Air Outlet	1 per container	Inside container / exhausting from one end	85	89	88	86	82	83	80	77	90
Radiator	8 per container	Roof mounted	79	84	82	76	76	72	66	62	81
Transformers	2	External	82	87	86	86	80	75	70	63	86

Table 4.3 – Sound Pressure Levels of Exhaust Outlet, Regenerated Noise, and Internal Levels within Generator Enclosure

Equipment	Quantity	Location	Sound Pressure Levels (SPL), dB								
			Octave Band Centre Frequencies, Hz (Unweighted values)								dB(A)
			63	125	250	500	1 k	2 k	4 k	8 k	
Unsilenced Exhaust Outlet ²	1 per container	Flue termination	123	124	114	106	97	97	97	89	111
Exhaust Outlet Attenuator Regenerated Noise ²	1 per container	Flue termination	64	64	64	64	64	60	55	51	68
Generator / inside container ³	1 per container	Inside container	81	91	89	98	100	101	100	106	109

Table 4.4 – Insertion Losses and Sound Reduction Indices Applied in the Noise Model

Component	Attenuation Performance Octave Band Centre Frequencies, Hz							
	63	125	250	500	1 k	2 k	4 k	8 k
Container (sound reduction indices)	15	19	23	31	40	48	52	52
Air Intake and Air Outlet Attenuators (insertion losses)	13	17	27	27	28	28	28	28
Exhaust Outlet (insertion losses)	55	64	66	65	64	62	60	61

2 - Sound pressure recorded at a distance of 1m and at an angle of 90° from the exhaust outlet opening

3 - Combination of reverberant and direct sound pressure levels

4.1.3 Predicted Noise Emissions

The noise predictions in this report have been made using a noise model which has been constructed using the CadnaA® software package, a commonly used 3-D noise mapping software that implements a wide range of national and international standards, guidelines and calculation algorithms, including those set out in ISO 9613-2:1996. A full explanation of the noise modelling is provided in **Appendix C**, along with images and noise maps/results from the model.

The model has been set up to reflect the site plan in **Figure 2.2** and the noise sources as described in **Section 4.1.2**.

Figure C.2 in **Appendix C** shows the predicted specific noise levels from all of the plant operating simultaneously, at a height of 4m to represent 1st floor windows at residential receptors. **Figures C.3** and **C.4** show views focused on NSR 1 and NSR 2 respectively.

As per **Appendix B.4**, a rating level penalty could be applied when assessing in accordance with BS 4142:2014+A1:2019

- **Tonality** – the equipment proposed typically emits noise over distance that is perceived as low frequency/broadband nature, without mid-to-high frequency tones/sound energy. A low frequency hum may be heard with emphasis at around 63 to 125 Hz. However, assessing in accordance with the Joint Nordic Method would require level differences in adjacent one-third octave bands of at least 15 dB between 25 Hz and 125 Hz to be defined as a low frequency tone. PJA has not observed differences between bands of greater than 15 dB when conducting measurements of sites with plant of this nature in operation. Therefore, no tonality penalty is applied.
- **Impulsivity** – no penalty as fans (the noise generating component) do not generally generate impulsive noises (and this was not noted when studying a similar facility).
- **Intermittency** – no penalty, the source is considered to be on for 100% of the reference time interval and thus an intermittency correction should *not be applied*.⁴
- **Other sound characteristics** – no penalty, as the noise source is in a heavily industrial area, the characteristics of the noise are unlikely to be distinctive compared to existing industrial noise.

4 - "There is scope for various interpretations of 'intermittency', and the word is not defined in BS 4142. Its presence should be considered in the context of the reference time interval and in conjunction with any 'on-time' correction. If a source is considered to be on for 100% of the reference time interval, an intermittency correction should not, therefore, be applied."

Table 4.3 shows the rating level 1m outside the worst affected residential windows at each NSR area in comparison to the daytime background sound level (when the plant would mostly likely operate).

Table 4.3 – Predicted noise levels and comparison with the daytime representative background sound level

Location	Period	Specific Noise Level L _{Aeq,Tr} (dB)	Rating Level Penalties (dB)	Rating Level L _{Ar,Tr} (dB)	Background Sound Level L _{A90,T} (dB)	Difference (dB)
NSR 1	Daytime (07:00 – 23:00) Tr = 1 hour	39	0	39	57	-18
NSR 2		43	0	43		-14

Table 4.4 shows the rating level in comparison to the *nighttime* background sound level.

Table 4.4 – Predicted noise levels and comparison with the nighttime representative background sound level

Location	Period	Specific Noise Level L _{Aeq,Tr} (dB)	Rating Level Penalties (dB)	Rating Level L _{Ar,Tr} (dB)	Background Sound Level L _{A90,T} (dB)	Difference (dB)
NSR 1	Nighttime (23:00 – 07:00) Tr = 15-minutes	39	0	39	42	-3
NSR 2		43	0	43		+1

4.1.4 Analysis

4.1.4.1. BS 4142 Assessment

Overnight at NSR 2, the rating level is 1 dB above the representative background sound level.

BS 4142 guidance suggests that a rating level exceeding the background by 5 dB could be an indicator of an adverse impact depending on the context.

For context, BS 4142 also states “where background sound levels and rating levels are low, absolute levels might be as, or more, relevant than the margin by which the rating level exceeds the background. This is especially true at night”.

For context, Annex G.1 of BS 8233:2014 suggests that “if partially open windows were relied upon for background ventilation, the insulation would be reduced to approximately 15 dB”.

Studies by Napier University ⁵ show that the sound insulation for partially open windows can be higher when open far enough to provide normal levels of background ventilation. The research shows that the typical attenuation of side hung, top hung, and bottom hung windows that are open with a free area of 0.2 m² is 18 – 19 dB D_{n,e,w}, with a relatively high performance at low frequencies (31.5, 63, and 125 Hz).

5 - Napier University. NANR116: ‘Open/Closed Window Research’ Sound Insulation through Ventilated Domestic Windows. (2007)

However, assuming as a worst-case that the performance is 15 dB, an external specific noise level of 43 dB would equate to an internal level of 28 dB. This would meet nighttime internal noise level targets (of 30 dB $L_{Aeq,8hrs}$) from BS 8233:2014 and WHO guidelines.

Furthermore, the operation of the site is not constant or regular, it is a backup site which will only produce the predicted noise emissions during periods of peak demand and/or short supply, for up to a couple of hours at a time.

The context of the development in what is already an extensive industrial area is also not considered unusual, i.e., the character of the noise would unlikely be distinguishable by residents to be from the particular site in question from the other noise generating sites in the area.

Therefore, the level of impact from noise in the operational phase of the development on local residents is expected to be acceptably low.

4.1.4.2. Comparison to Previous Assessments

The predicted specific noise levels from the current assessment are 39 dB L_{Aeq} at NSR 1 and 43 dB L_{Aeq} at NSR 2, both rounded to 0 decimal places.

For comparison, the previous assessments reported the following:

- Royal HaskoningDHV (2017) – 44 dB L_{Aeq} at NSR 1 and 46 dB L_{Aeq} at NSR 2 (see **Section 3.1.1**).
- ParkerJones Acoustics (2024, Revision 1) – 39 dB L_{Aeq} at NSR 1 and 44 dB L_{Aeq} at NSR 2 (see **Section 3.1.2**).

Accordingly, the current predictions are 5 dB lower than the 2017 assessment at NSR 1, 3 dB lower than 2017 at NSR 2, equal to the 2024 level at NSR 1, and 1 dB lower than 2024 at NSR 2.

These results demonstrate a clear reduction in predicted noise emissions compared with the earlier 2017 layout, and a modest further improvement relative to the 2024 (Revision 1) configuration.

In all cases, the predicted specific noise levels remain well below the representative background levels established by Royal HaskoningDHV in 2017, indicating a low likelihood of adverse impact in accordance with BS 4142:2014 + A1:2019.

The comparison confirms that the revised layout would not result in any material increase in noise impact relative to the previously approved schemes and can therefore be considered acoustically equivalent or better.

4.2 Construction Noise

PJA has previously produced a Construction Noise/Vibration Assessment report ⁶ (on the 18th of February 2022) as part of approved planning application APP/21/00809. This was based on assessing against noise and vibration limits identified by Natural England in sensitive areas within the *Solent Wader and Brent Goose Strategy Candidate sites*.

The proposed changes in site layout/quantity of mechanical plant are not anticipated to change the construction methods.

Therefore, the aforementioned report remains valid and applicable to this application.

The conclusions were that the noise and vibration limits set by Natural England were unlikely to be exceeded, but nonetheless, a Construction Noise Management Plan (detailed in the report) should be followed to ensure this is the case and to minimise noise emissions using Best Practicable Means to mitigate and offset the impact as much as is reasonably possible.

4.3 Conclusions

In summary, the predicted specific noise levels from the proposed layout are 39 dB at NSR 1 and 43 dB at NSR 2, which are 5 dB and 3 dB lower respectively than the corresponding levels predicted in the 2017 Royal HaskoningDHV assessment, and equivalent or up to 1 dB lower than those predicted in PJA's 2024 (Revision 1) assessment.

The results therefore confirm that the revised layout would not result in any material increase in noise impact relative to the previously approved schemes and can be considered acoustically equivalent or better.

At these levels, noise emissions during peak operation are considered unlikely to result in any adverse impact on the nearest residential receptors, remaining at least 14 dB below typical daytime background levels. The predicted levels would also satisfy the internal ambient noise targets of BS 8233:2014 within nearby dwellings, even with partially open windows.

The findings of the Construction Noise and Vibration Assessment previously issued by PJA (18 February 2022, under application APP/21/00809) also remain valid. The proposed amendments to the layout and plant arrangement would not materially alter the anticipated construction methods, and the earlier conclusions remain applicable — namely, that the identified noise and vibration limits are unlikely to be exceeded, provided that the Construction Noise Management Plan (as detailed in that report) is implemented and that Best Practicable Means continue to be applied to minimise emissions.

6 - https://planningpublicaccess.havant.gov.uk/online-applications/files/BD94D4F116777A8E93E3B9560AA82389/pdf/APP_21_00809-ADDITIONAL_CONSTRUCTION_NOISE_AND_VIBRATION_ASSESSMENT-1619804.pdf

Appendix A – Acoustic Terminology and Concepts

A.1 – Glossary

Table A.1 – Glossary of acoustic terminology

Term	Description
dB (decibel)	The scale on which sound pressure level is expressed. It is defined as 20 times the logarithm of the ratio of the root-mean-square pressure of the sound and a reference pressure (2×10^{-5} Pa).
dB(A)	A-weighted decibel. This is a measure of the overall level of sound across the audible spectrum with a frequency weighting (i.e., 'A' weighting) to compensate for the varying sensitivity of the human ear to sound at different frequencies.
Frequency	Sound can occur over a range of frequencies extending from the very low, such as the rumble of thunder, up to the very high such as the crash of cymbals. Sound is generally described over the frequency range from 63Hz to 4000Hz (4kHz). This is roughly equal to the range of frequencies on a piano.
$L_{Aeq,T}$	L_{Aeq} is defined as the notional steady sound level which, over a stated period of time, would contain the same amount of acoustical energy as the A-weighted fluctuating sound measured over that period. This parameter is typically considered as a good representation of the 'average' overall noise level. It is referred to technically as the A-weighted equivalent continuous sound level and is a dB(A) as defined above.
$L_{A90,T}$	The A-weighted noise level that is exceeded for 90% of the measurement period T. This parameter is often considered as the 'average minimum level'.
$L_{A10,T}$	The A-weighted noise level that is exceeded for 10% of the measurement period T. This parameter is often considered as the 'average maximum level';
$L_{AFmax,T}$	The maximum A-weighted noise level during the measurement period T.

A.2 – Subjective Changes in Noise Level

Table A.2 – Subjective loudness from an increase or decrease in sound pressure level

Change in sound pressure level	Relative change in sound power energy (multiplier)		Change in apparent subjective loudness (for mid-frequency range)
	Decrease	Increase	
3 dB	1/2	2	'Just perceptible'
5 dB	1/3	3	'Clearly noticeable'
10 dB	1/10	10	'Half or twice as loud'
20 dB	1/100	100	'Much quieter, or louder'

Appendix B – Relevant Planning Policies and Guidelines

B.1 – National Planning Policy Framework (NPPF)

The National Planning Policy Framework (NPPF) sets out the Government's planning policies for England and how these are expected to be applied. The NPPF provides a framework within which local people and their council can produce their own distinctive local and neighbourhood plans. With explicit reference to noise, the NPPF states that *"Planning policies and decisions should contribute to and enhance the natural and local environment by ... preventing new and existing development from contributing to, being put at unacceptable risk from ... noise pollution"*.

B.2 - Noise Policy Statement for England (NPSE)

The NPPF refers to the Noise Policy Statement for England (NPSE), which applies to most forms of noise including environmental noise. The NPSE sets out the long-term vision of Government policy which is to *"Promote good health and a good quality of life through the effective management of noise within the context of Government policy on sustainable development."* It aims that *"Through the effective management and control of environmental, neighbour and neighbourhood noise within the context of Government policy on sustainable development:*

- *avoid significant adverse impacts on health and quality of life;*
- *mitigate and minimise adverse impacts on health and quality of life; and*
- *where possible, contribute to the improvement of health and quality of life."*

The use of the terms *"significant adverse"* and *"adverse"* are key phrases within the NPSE. The guidance establishes the concept of how the level of adverse effect on health and quality of life can be referenced including:

- **NOEL – No Observed Effect Level** - This is the level below which no effect can be detected. In simple terms, below this level, there is no detectable effect on health and quality of life due to the noise.
- **LOAEL – Lowest Observed Adverse Effect Level** - This is the level above which *adverse* effects on health and quality of life can be detected.
- **SOAEL – Significant Observed Adverse Effect Level** - This is the level above which *significant adverse* effects on health and quality of life occur.

Under the first aim of the NPSE (*"avoid significant adverse impacts on health and quality of life"*), an impact in line with SOAEL should be avoided. Under the second aim (*"mitigate and minimise adverse impacts on health and quality of life"*), where the impact lies somewhere between LOAEL and SOAEL, requiring that all reasonable steps are taken to mitigate and minimise adverse effects on health and quality of life while also taking into account the guiding principles of sustainable development, but does not mean that such adverse effects cannot occur.

B.3 - Planning Practice Guidance on Noise (PPG-N)

The Planning Practice Guidance on Noise (PPG-N) is part of a suite of web-based guidance which is intended to support the implementation of the policies in the NPPF and the NPSE.

It aids in expanding on the definitions from the NPSE of NOEL, LOAEL and SOAEL, by linking these terms to 'examples of outcomes', i.e., changes in behaviour and/or attitude to noise. The table below summarises the guidance from PPG-N in this regard.

Table B.1 – Noise exposure hierarchy based on the likely average response – adapted from PPG-N

Perception	Examples of outcomes	Increasing effect level	Action
NOEL - No Observed Effect Level ¹			
Not noticeable	No Effect	No Observed Effect	No specific measures required
Noticeable and not intrusive	Noise can be heard but does not cause any change in behaviour or attitude. Can slightly affect the acoustic character of the area but not such that there is a perceived change in the quality of life.	No Observed Adverse Effect	No specific measures required
LOAEL - Lowest Observed Adverse Effect Level			
Noticeable and intrusive	Noise can be heard and causes small changes in behaviour and/or attitude, e.g., turning up the volume of television; speaking more loudly; where there is no alternative ventilation, having to close windows for some of the time because of the noise. Potential for some reported sleep disturbance. Affects the acoustic character of the area such that there is a perceived change in the quality of life.	Observed Adverse Effect	Mitigate and reduce to a minimum
SOAEL - Significant Observed Adverse Effect Level			
Noticeable and disruptive	The noise causes a material change in behaviour and/or attitude, e.g., avoiding certain activities during periods of intrusion; where there is no alternative ventilation, having to keep windows closed most of the time because of the noise. Potential for sleep disturbance resulting in difficulty in getting to sleep, premature awakening and difficulty in getting back to sleep. Quality of life diminished due to a change in the acoustic character of the area.	Significant Observed Adverse Effect	Avoid
Noticeable and very disruptive	Extensive and regular changes in behaviour and/or an inability to mitigate the effect of noise leading to psychological stress or physiological effects, e.g., regular sleep deprivation/awakening; loss of appetite, significant, medically definable harm, e.g., auditory and non-auditory	Unacceptable Adverse Effect	Prevent
¹ This line is an assumption of the adverse effect level and is not explicitly referenced by PPG-N, though this appears to be a safe assumption.			

B.4 - BS 4142:2014

BS 4142:2014 'Methods for rating and assessing industrial and commercial sound' is intended to be used to assess the potential adverse impact of sound of an industrial and/or commercial nature, at nearby noise-sensitive receptor (NSR) locations within the context of the existing sound environment.

B.4.1 - Definitions

BS 4142:2014 provides the following definitions which are relevant at this pre-construction stage of assessment:

- **Background Sound Level, $L_{A90,T}$:** A-weighted sound pressure level that is exceeded by the residual sound at the assessment location for 90% of a given interval, T, measured using time weighting F and quoted to the nearest whole number of decibels.
- **Rating Level, L_{Ar,T_r} :** Specific sound level plus any adjustment for the characteristic features of the sound.
- **Reference Time Interval, T_r :** Specified interval over which the specific sound level is determined. This is 60-minutes during the day (07:00 – 23:00) and 15-minutes at night (23:00 – 07:00).
- **Specific Sound Level, $L_s = L_{Aeq,T_r}$:** Equivalent continuous A-weighted sound pressure level produced by the specific sound source at the assessment location over a given reference time interval, T_r .
- **Specific Sound Source:** Sound source being assessed.

The BS 4142:2014 definition of sound of an industrial and/or commercial nature includes "sound from fixed installations which comprise mechanical and electrical plant and equipment". The scope of BS 4142:2014 is not intended for sound from the passage of vehicles on public roads; people; and 'other sources falling within the scopes of other standards or guidance'.

B.4.2 - Specific Sound Level

The specific sound level L_s is the equivalent continuous A-weighted sound pressure level produced by the specific sound source at the assessment location over a given reference time interval, T_r , of 60-minutes during the day (07:00 – 23:00) and 15-minutes at night (23:00 – 07:00).

B.4.3 - Rating Level

The rating level L_{Ar,T_r} is the specific sound level L_s plus any 'penalties' which account for the characteristic features of the sound.

BS 4142:2014 provides the following with respect to the application of penalties to account for "the subjective prominence of the character of the specific sound at the noise-sensitive locations and the extent to which such acoustically distinguishing characteristics will attract attention".

- **Tonality** – For sound ranging from not tonal to predominantly tonal the Joint Nordic Method gives a correction of between 0 dB and +6 dB for tonality. Subjectively, this can be converted to a penalty of 2 dB for a tone which is just perceptible at the noise receptor, 4 dB where it is clearly perceptible and 6 dB where it is highly perceptible;

- **Impulsivity** – A correction of up to +9 dB can be applied for sound that is highly impulsive, considering both the rapidity of the change in sound level and the overall change in sound level. Subjectively, this can be converted to a penalty of 3 dB for impulsivity which is just perceptible at the noise receptor, 6 dB where it is clearly perceptible, and 9 dB where it is highly perceptible;
- **Intermittency** – When the specific sound has identifiable on/off conditions, the specific sound level ought to be representative of the time period of length equal to the reference time interval which contains the greatest total amount of on time. If the intermittency is readily distinctive against the residual acoustic environment, a penalty of 3 dB can be applied; and
- **Other Sound Characteristics** – Where the specific sound features characteristics that are neither tonal nor impulsive, though otherwise are readily distinctive against the residual acoustic environment, a penalty of 3 dB can be applied."

PJA consider the word 'perceptible' to be important, and variable depending on the context of a site. For example at a site with a relatively high background sound level of 50 dB(A), an 'impulsive' sound source with a specific sound level of 30 dB(A) at an NSR is unlikely to be perceptible and should probably not be penalised.

However, the same source at a site with a lower background level of 30 dB(A) would be perceptible, and therefore a penalty of 3 or 6 dB could be applied to the rating level, with possibly a 9 dB penalty being applied if the specific sound level were to rise from 30 to 40 dB(A). Therefore the context is important in applying rating level penalties.

B.4.4 - Background Sound Level

BS 4142:2014 states that "in using the background sound level in the method for rating and assessing industrial and commercial sound it is important to ensure that values are reliable and suitably represent both the particular circumstances and periods of interest. For this purpose, the objective is not simply to ascertain a lowest measured background sound level, but rather to quantify what is typical during particular time periods."

BS 4142:2014 further states that "a representative level ought to account for the range of background sound levels and ought not automatically to be assumed to be either minimum or modal value". Hence BS 4142:2014 does not provide a 'black and white' method of obtaining the assessment level for background sound $L_{A90,T}$. Note that it is standard practice that the $L_{A90,T}$ is determinable from the results of a baseline sound survey conducted at positions representative of sound levels at the nearest or worst affected NSRs.

B.4.5 - Assessment of Adverse Impact

The assessment of adverse impact contained in BS 4142:2014 is undertaken by comparing the rating level $L_{A,r,Tr}$ to the measured representative background sound level $L_{A90,T}$ outside the sensitive receptor location.

The significance of the impact of an industrial or commercial sound source depends on both the margin by which the rating level $L_{A,r,Tr}$ exceeds the background sound level $L_{A90,T}$ and the context in which the sound occurs. It is therefore essential to place the sound in context. But in general, "the lower the rating level is relative to the measured background sound level, the less likely it is that the specific sound source will have an adverse impact or a significant adverse impact. Where the rating level does not exceed the background sound level, this is an indication of the specific sound source having a low impact, depending on the context."

Appendix C – Predicted Noise Emissions

The noise predictions within this report have been undertaken using the proprietary software CadnaA® by DataKustik, a 3-D noise mapping package which implements a wide range of national and international standards, guidelines and calculation algorithms, including those set out in ISO 9613-2:1996.

All of the objects within the model (buildings, roads, barriers, foliage, etc) have been imported from OpenStreetMap. The heights of the buildings and roads have been based upon Google Earth Pro, using the 3D view to be able to measure the elevation heights at the tops of objects, and then inserting this manually into the model. Lastly, the scaled site plan, floor plan, and elevation for the proposed development have been accounted for in the model.

The noise model has been used to predict the resulting L_{Aeq} *specific* noise emissions from the proposed plant.

The noise model has assumed:

- a maximum reflection factor of three where buildings and barriers are assumed to have a 'smooth' reflective façade, as a worst-case;
- a ground absorption factor of 0 on the site and any roads/tarmacked areas, and 1 in greenfield land.
- receptor heights on the façade at ground floor (1.5m) and top floor (4m) levels;
- atmospheric sound absorption based upon a temperature of 10°C and a humidity level of 70%, as per Table 2 of ISO 9613-2:1996;
- downwind propagation, i.e., a wind direction that assists the propagation of sound from source to receptor, as a worst-case.

The images on the following pages contain the results of the mapping, showing the predicted specific noise levels (rating level penalties are not included).

Figure C.1 – 3D view of the model setup

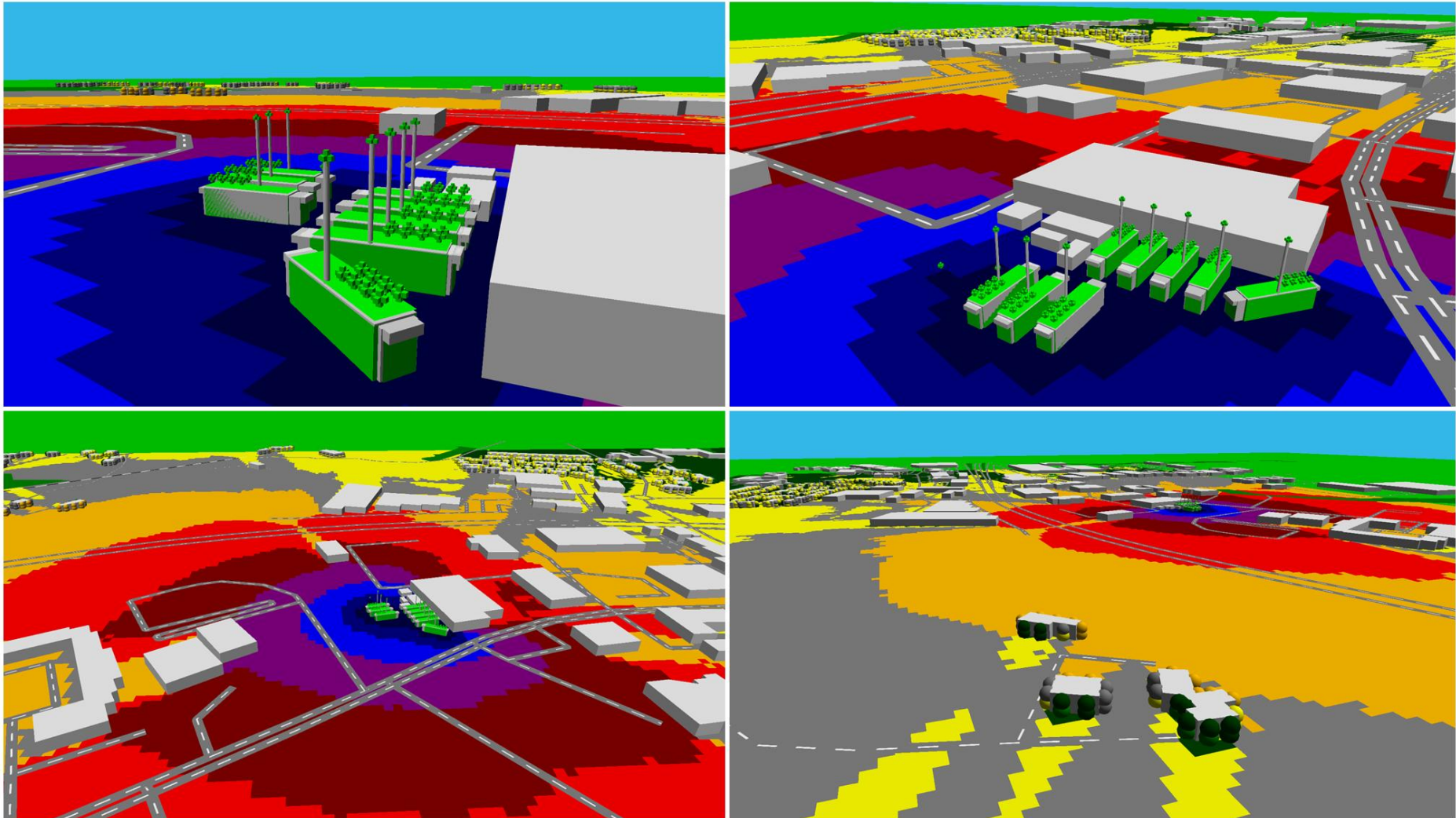


Figure C.2 – Predicted specific noise levels (dB L_{Aeq}) – all plant operating simultaneously/full capacity – wide view

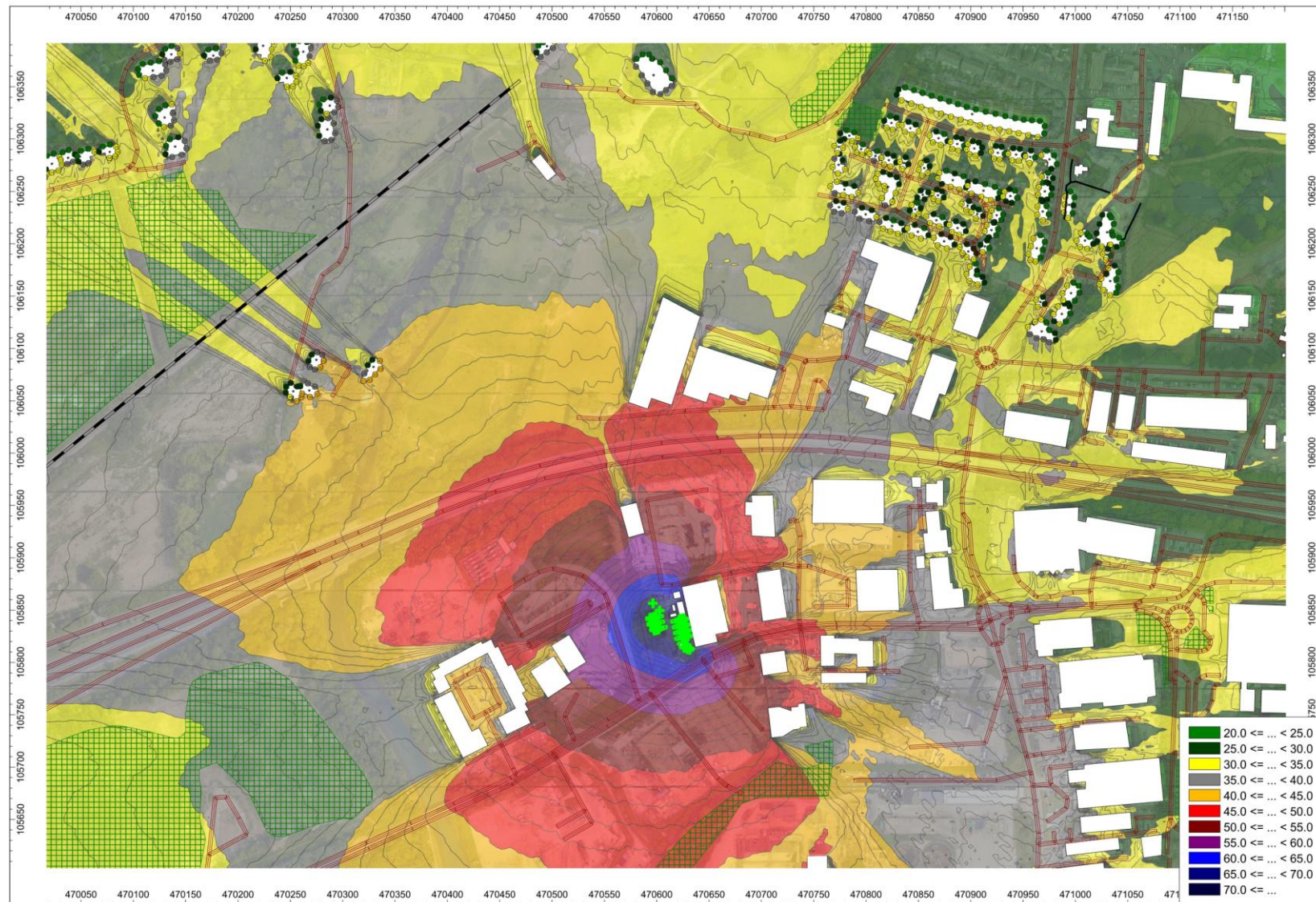


Figure C.3 – Predicted specific noise levels (dB L_{Aeq}) – all plant operating simultaneously/full capacity – NSR 1

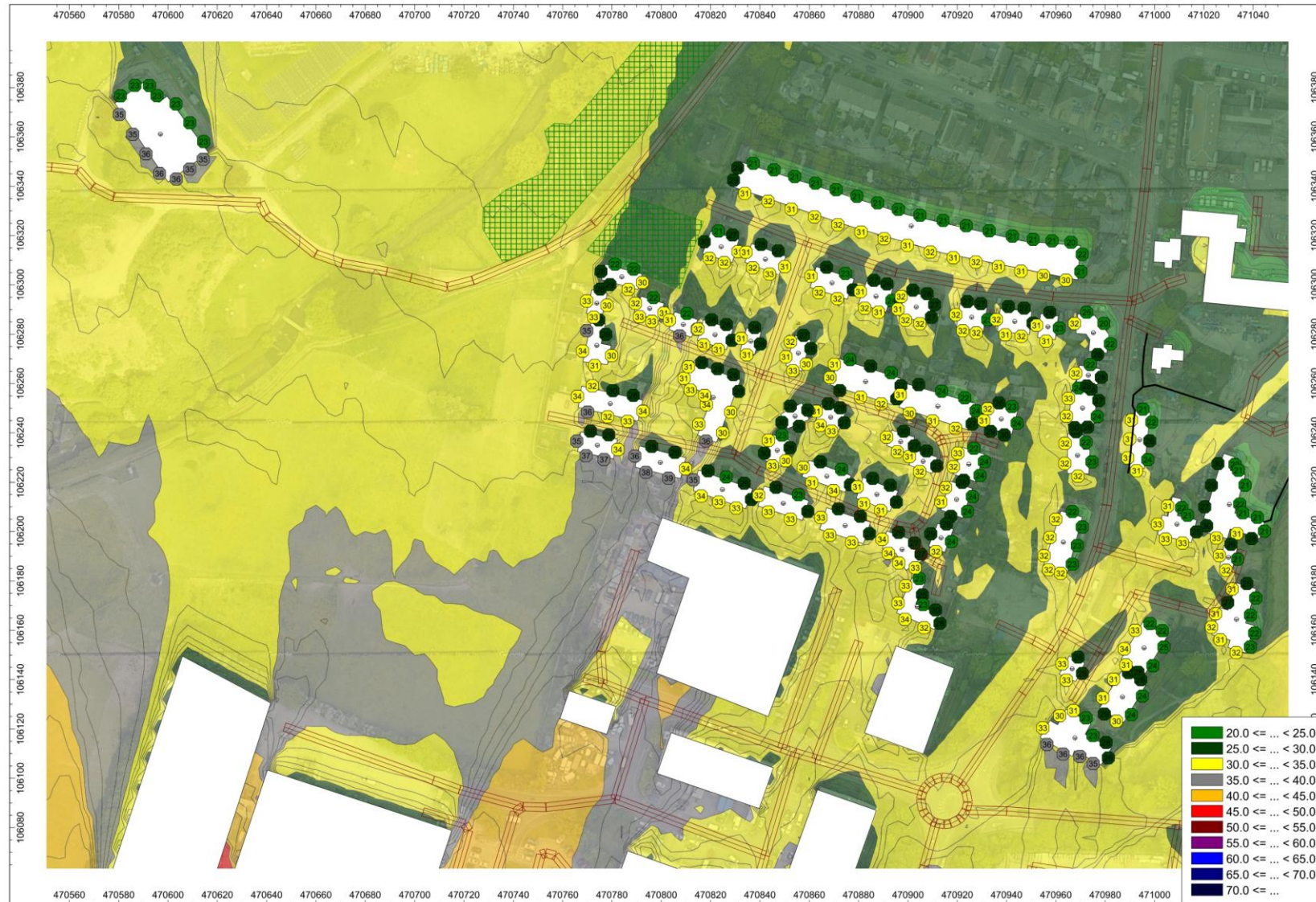
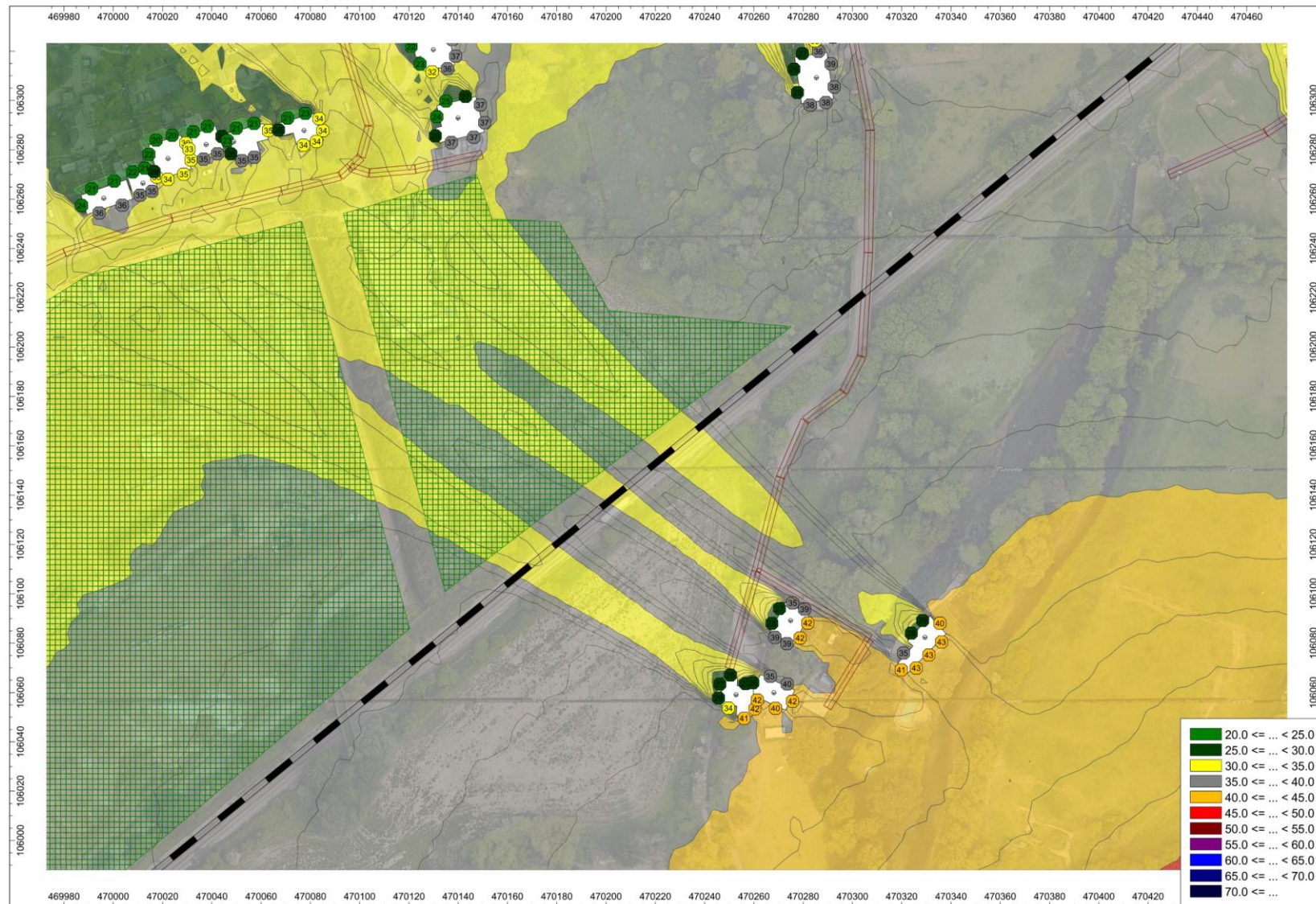


Figure C.4 – Predicted specific noise levels (dB L_{Aeq}) – all plant operating simultaneously/full capacity – NSR 2



Appendix D - Author Qualifications

This report has been produced by Chris Parker-Jones, the director and primary acoustic consultant at ParkerJones Acoustics. Chris holds the following qualifications:

- MIOA (Member of the Institute of Acoustics)
- BSc in Music Systems Engineering from the University of the West of England – 1st Class
- MSc in Sound and Vibration Studies from the University of Southampton - Distinction

Chris has worked as an acoustic consultant for various companies since July 2011.



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